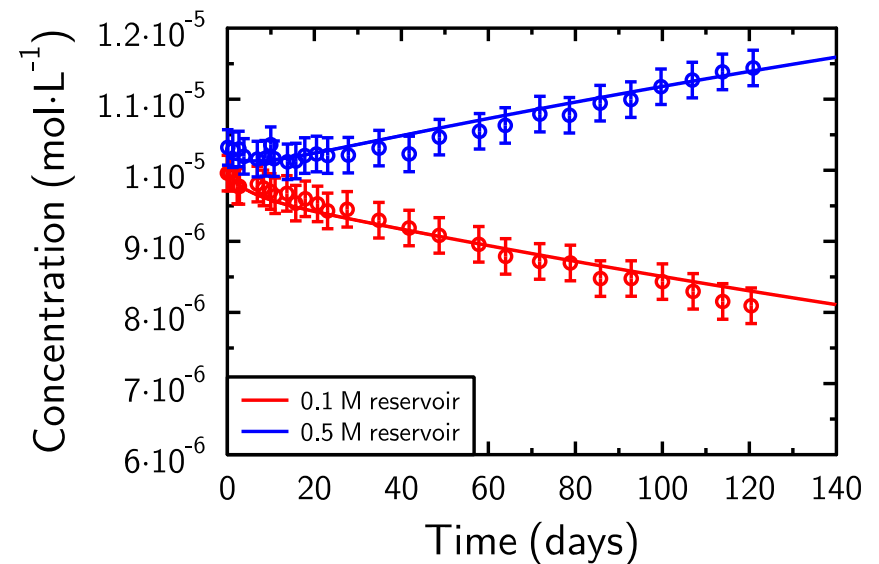
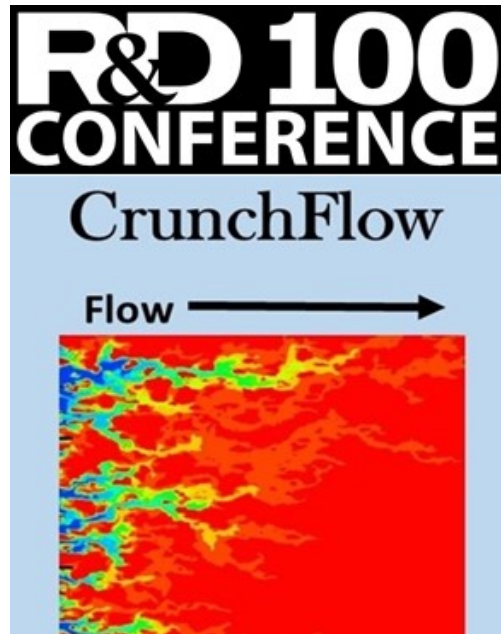


Introduction to Reactive Transport with CrunchTope

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Reactive Transport Equations

Fully Kinetic Approach

$$\frac{\partial(\phi S_L C_i)}{\partial t} = \nabla \cdot (\phi S_L D_i^* \nabla C_i) - \nabla \cdot (\mathbf{q} C_i) - \sum_{r=1}^{N_r} \nu_{ir} R_r - \sum_{m=1}^{N_m} \nu_{im} R_m - \sum_{l=1}^{N_g} \nu_{il} R_l$$

Accumulation
Term

Dispersion-
Diffusion

Advection

Aqueous
Reactions

Mineral
Reactions

Gas
Reactions


Partial Equilibrium Approach

$$\frac{\partial(\phi S_L \Psi_i)}{\partial t} = \nabla \cdot (\phi S_L D_i^* \nabla \Psi_i) - \nabla \cdot (\phi S_L \mathbf{v} \Psi_i) - \sum_{r=1}^{N_r} \nu_{ir} R_r - \sum_{m=1}^{N_m} \nu_{im} R_m - \sum_{l=1}^{N_g} \nu_{il} R_l$$

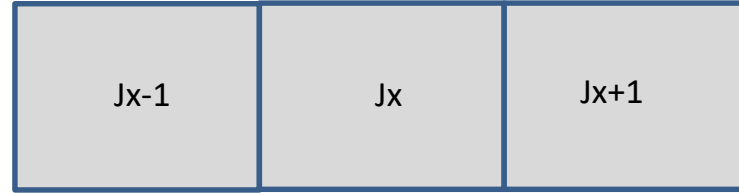
Total
Concentration

Secondary
Species

Rewritten with
Primary Species

$$\psi_i = C_i + \sum_{l=1}^{N_s} \nu_{i,l} C_l = C_i + \sum_{l=1}^{N_s} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right]$$


Reactive Transport Equations: Numerical



Accumulation
Term

Dispersion-
Diffusion

Advection

Aqueous
Reactions

$$\phi S_L \frac{[\psi_{i,jx}^{n+1} - \psi_{i,jx}^n]}{\Delta t} - \phi S_L D \frac{[\psi_{i,jx-1}^{n+1} - 2\psi_{i,jx}^{n+1} + \psi_{i,jx+1}^{n+1}]}{\Delta x^2} + \phi S_L v \frac{[\psi_{i,jx-1}^{n+1} - \psi_{i,jx}^{n+1}]}{\Delta x} + \sum_{r=1}^{N_r} [R_{i,r}^{n+1}] = 0$$

Rewrite Ψ in terms of primary species concentrations

$$\begin{aligned} & \frac{\phi S_L}{\Delta t} \left[\left(C_i + \sum_{l=1}^{N_s} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right] \right)_{i,jx}^{n+1} - \psi_{i,jx}^n \right] + \sum_{r=1}^{N_r} [R_{i,r}^{n+1}]_{jx} && \text{Accumulation + Reaction Terms} \\ & \cdot + \frac{\phi S_L v}{\Delta x} \left[\left(C_i + \sum_{l=1}^{N_s} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right] \right)_{i,jx}^{n+1} - \left(C_i + \sum_{l=1}^{N_s} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right] \right)_{i,jx-1}^{n+1} \right] && \text{Transport Terms} \\ & \cdot - \frac{\phi S_L D}{\Delta x^2} \left[\left(C_i + \sum_{l=1}^{N_s} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right] \right)_{i,jx-1}^{n+1} - 2 \left(C_i + \sum_{l=1}^{N_s} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right] \right)_{i,jx}^{n+1} + \left(C_i + \sum_{l=1}^{N_s} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right] \right)_{i,jx+1}^{n+1} \right] = 0 \end{aligned}$$

SHORT COURSE EXERCISES

Short Course Exercises

Introduction to speciation

- Example using the carbonate system featuring various constraints
- Stable isotopes of carbon (^{12}C and ^{13}C) implemented to demonstrate equilibrium fractionation

Advective transport

- Introduce a non-reactive tracer into an advective flow field
- Investigate numerical dispersion

Diffusive transport

- Introduce a non-reactive tracer into a purely diffusive transport problem
- No-flux versus Dirichlet boundary conditions

Multicomponent diffusion

- Concept of charged species diffusing at different rates and electrochemical migration
- Stable isotopes of Cl are implemented to consider the influence of diffusive fractionation

Transverse dispersion

- Example based on a recent 2D dispersion experiment, including multi-ion diffusion in an advective flow field

Ion exchange

- Introduce ion exchange of cesium in a 1D sediment column with competing Na^+

Surface complexation

- Surface complexation of zinc on iron-hydroxide (PHREEQc example 8)

CO_2 attack on reservoir rocks

- Diffusion of gas and flow of water, with variable liquid saturations and multi-mineral nucleation, precipitation, and dissolution

Calcite precipitation with isotopes

- Simulation of stable isotope kinetic fractionation of calcium during carbonate precipitation

Two-dimensional flow fields

- Xie et al (2015) benchmark on porosity and permeability change due to mineral reaction

Diffusion in clay

- Tournassat & Steefel, 2016

Inverse modeling with PEST-CrunchFlow

- Steefel et al, 2003

CrunchTope Files

1) Executable: `CrunchTope.exe`

2) Input file: `name.in`

1) Database(s): `name.dbs`

```
TITLE
Cs exchange on Hanford sediments: Experiment 3
END

RUNTIME
time_units          hours
timestep_max        0.1
timestep_init       0.00001
time_tolerance      0.01
solver              gmres
preconditioner      ilu
precondition_level  1
lag_activity        on
debye-huckel        on
database_sweep      off
speciate_only       false
hindmarsh           true
gimrt               true
courant_number      1.0
density_module      sodium_nitrate
graphics            kaleidagraph
screen_output       50
database            HanfordTanksColumnFit3Site-GT.dbs
save_restart        Column3NaN03Flush1.rst
later_inputfiles    ShortCourse12b.in ShortCourse12c.in
END

OUTPUT
time_units          hours
spatial_profile     19.25
```

```
temperature points' 8 0. 25. 60. 100. 150. 200. 250. 300.
'Debye-Huckel adh'  0.4939 0.5114 0.5465 0.5995 0.6855 0.7994 0.9593 1.2180
'Debye-Huckel bdh'  0.3253 0.3288 0.3346 0.3421 0.3525 0.3639 0.3766 0.3925
'Debye-Huckel bdt'  0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
'H2O' 3.0 0.0 18.0153
'Ag+' 2.5 1.0 107.8682
'Al+++ ' 9.0 3.0 26.9815
'Am+++ ' 5.0 3.0 243.0000
'Ar(aq)' 3.0 0.0 39.9480
'Au+' 4.0 1.0 196.9665
'B(OH)3(aq)' 3.0 0.0 61.8330
'Ba++' 5.0 2.0 137.3270
'Be++' 8.0 2.0 9.0122
'Br-' 3.0 -1.0 79.9040
'Ca++' 6.0 2.0 40.0780
'Cd++' 5.0 2.0 112.4110
'Ce+++ ' 9.0 3.0 140.1150
'Cl-' 3.0 -1.0 35.4527
```

CrunchTope Files

OUTPUT

```
time_units      hours
spatial_profile 16.0 32.0
time_series     Rolle.out 11 20 1
time_series_print K+ Mg++ Cl-
time_series_interval 1
END/
```

spatial_profile generated automatically
at times specified (16, 32 hours)

time_series saved every
time_series_interval in file `Rolle.out`

time_series_print writes species
specified in file `Rolle.out`

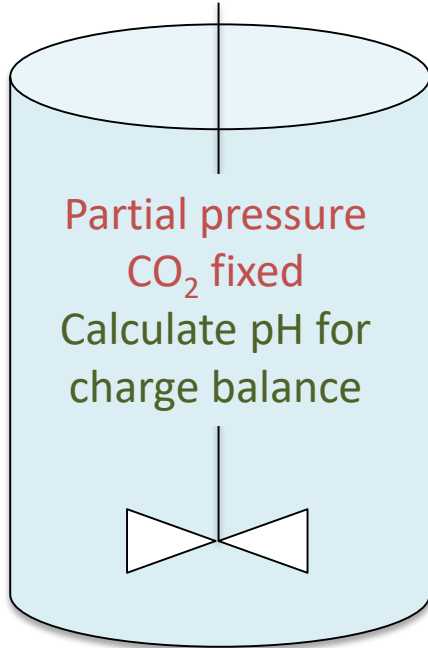
Spatial profile files include:

1. totcon#.tec total concentrations in solution
2. pH#.tec solution pH
3. conc#.tec log concentrations of individual species
4. rate#.tec mineral reaction rates (mol/L(bulk)/s)
5. aq_rate#.tec aqueous reaction rates (mol/L/s)
6. volume#.tec mineral volume fraction (dimensionless)
7. porosity#.tec (dimensionless)
8. velocity#.tec Darcy flux ($\text{m}^3/\text{m}^2/\text{yr}$)
9. toperatio_aq#.out per mil
10. toperatio_min#.out per mil

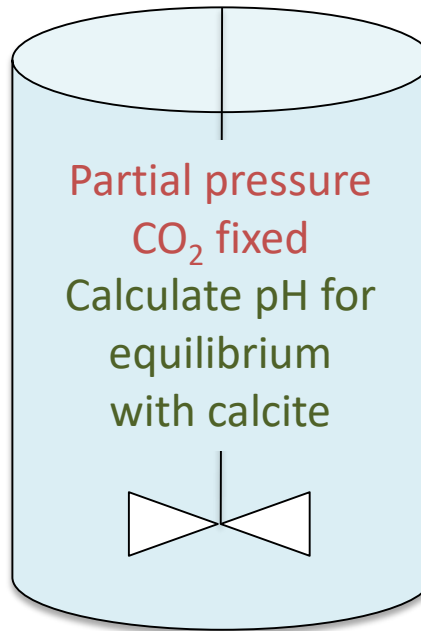
SPECIATION

Exercise 1: Carbonate Speciation

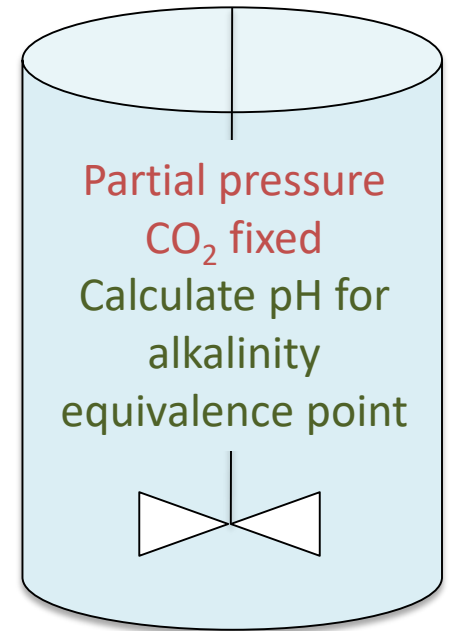
Condition: speciate 1



Condition: speciate 2



Condition: speciate 3



Input Blocks

```
RUNTIME
speciate_only    true
database_sweep  false
database         datacom_13C.dbs
graphics        tecplot
density_module   temperature
END
```

```
PRIMARY_SPECIES
H+
CO2(aq)
13CO2(aq)
Ca++
Na+
Cl-
END
```

```
GASES
CO2(g)
13CO2(g)
END
```

```
MINERALS
Calcite  -label default -rate -11.00
END
```

Log rate (mol/m²/s)



```
SECONDARY_SPECIES
HCO3-
H13CO3-
CaCl+
CaCl2(aq)
CaOH+
HCl(aq)
NaCl(aq)
NaOH(aq)
OH-
CO3—
13CO3--
CaCO3(aq)
Ca13CO3(aq)
CaHCO3+
CaH13CO3+
NaCO3-
Na13CO3-
NaHCO3(aq)
NaH13CO3(aq)
END
```

Stoichiometric Reaction Matrix

HOMOGENEOUS REACTIONS

Species	log K	Stoichiometric Coefficients					
		H+	CO2(aq)	13CO2(Ca++	Na+	Cl-
HCO3-	6.3414E+00	-1.00	1.00	0.00	0.00	0.00	0.00
H13CO3-	6.3390E+00	-1.00	0.00	1.00	0.00	0.00	0.00
CaCl+	7.0039E-01	0.00	0.00	0.00	1.00	0.00	1.00
CaCl2(aq)	6.5346E-01	0.00	0.00	0.00	1.00	0.00	2.00
CaOH+	1.2850E+01	-1.00	0.00	0.00	1.00	0.00	0.00
HCl(aq)	-6.9993E-01	1.00	0.00	0.00	0.00	0.00	1.00
NaCl(aq)	7.8213E-01	0.00	0.00	0.00	0.00	1.00	1.00
NaOH(aq)	1.4799E+01	-1.00	0.00	0.00	0.00	1.00	0.00
OH-	1.3991E+01	-1.00	0.00	0.00	0.00	0.00	0.00
CO3--	1.6666E+01	-2.00	1.00	0.00	0.00	0.00	0.00
13CO3--	1.6664E+01	-2.00	0.00	1.00	0.00	0.00	0.00
CaCO3(aq)	1.3350E+01	-2.00	1.00	0.00	1.00	0.00	0.00
Ca13CO3(aq)	1.3348E+01	-2.00	0.00	1.00	1.00	0.00	0.00
CaHCO3+	5.2986E+00	-1.00	1.00	0.00	1.00	0.00	0.00
CaH13CO3+	5.2961E+00	-1.00	0.00	1.00	1.00	0.00	0.00
NaCO3-	1.6157E+01	-2.00	1.00	0.00	0.00	1.00	0.00
Na13CO3-	1.6155E+01	-2.00	0.00	1.00	0.00	1.00	0.00
NaHCO3(aq)	6.1857E+00	-1.00	1.00	0.00	0.00	1.00	0.00
NaH13CO3(aq)	6.1832E+00	-1.00	0.00	1.00	0.00	1.00	0.00

Stoichiometric Reaction Matrix

MINERAL REACTIONS

Mineral	log K	Stoichiometric Coefficients					
		H+	CO2(aq	13CO2(Ca++	Na+	Cl-
Calcite	8.1957E+00	-2.00	1.00	0.00	1.00	0.00	0.00

GAS REACTIONS

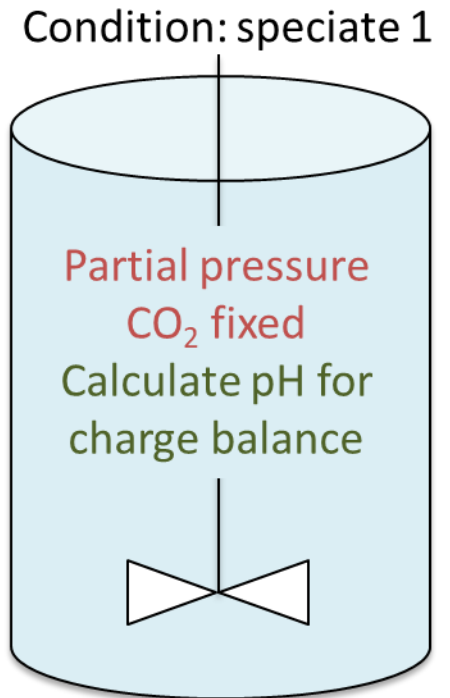
Gases	log K	Stoichiometric Coefficients					
		H+	CO2(aq	13CO2(Ca++	Na+	Cl-
CO2(g)	-1.4677E+00	0.00	1.00	0.00	0.00	0.00	0.00
13CO2(g)	-1.4680E+00	0.00	0.00	1.00	0.00	0.00	0.00

Condition Blocks

Label for condition used in INITIAL_CONDITIONS and BOUNDARY_CONDITIONS and PUMP

```
Condition      speciate1
!! Fix pCO2 and calculate pH based on charge balance
units          mol/kg
temperature    25.0
pH             charge
!!gas partial pressure in bars
CO2(aq)        CO2(g)      3.12E-04
13CO2(aq)      13CO2(g)     3.15E-06
Na+            0.01
Cl-            0.01
Ca++           0.00
END
```

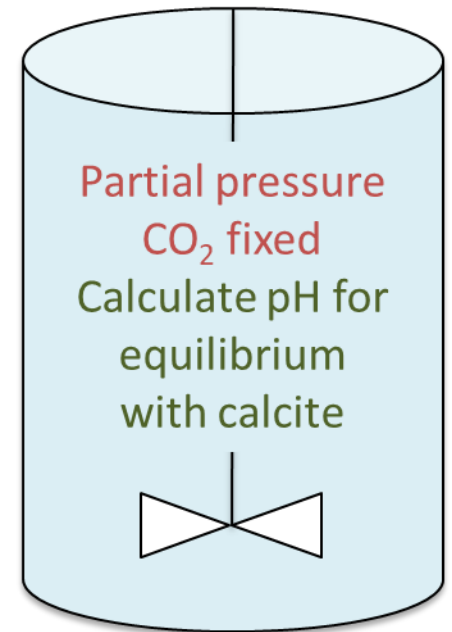
Gas partial pressure in bars



Condition Blocks

```
Condition      speciate2
!! Fix pCO2 and calculate pH based on calcite equilibrium
units          mol/kg
temperature    25.0
pH             Calcite
!! Gas partial pressure in bars
CO2(aq)        CO2(g)    3.12E-04
13CO2(aq)     13CO2(g)  3.15E-06
Na+            0.01
Cl-            charge
Ca++           0.01
END
```

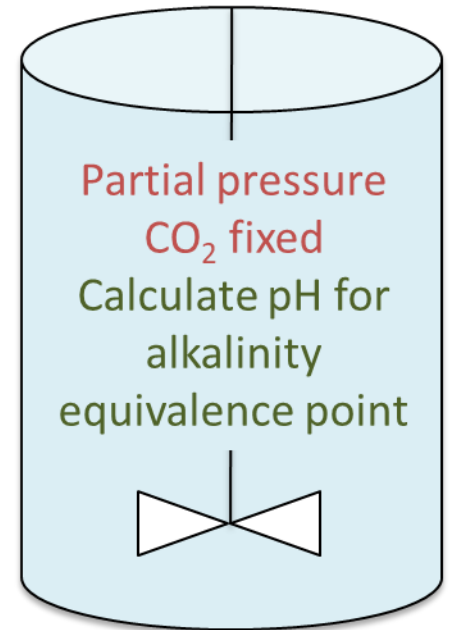
Condition: speciate 2



Condition Blocks

```
Condition    speciate3
!! Fix pCO2 and calculate pH based on alkalinity at the CO2
!!  equivalence point (alkalinity = 0.00)
units       mol/kg
temperature  25.0
H+          0.00
!! gas partial pressure in bars
CO2(aq)     CO2(g)    3.12E-04
13CO2(aq)   13CO2(g)   3.15E-06
Na+         0.01
Cl-         0.01
Ca++        0.00
END
```

Condition: speciate 3



Total Hydrogen = -Alkalinity

Discretization and Initial and Boundary Conditions

```
DISCRETIZATION
```

```
xzones 1 1.0
```

```
END
```

```
INITIAL_CONDITIONS
```

```
speciate1 1-1
```

```
END
```

NOTE: No boundary conditions needed for initial value problem

Minimum 3 grid cells required for a boundary value problem (with transport

Exercise 1: Carbonate Speciation

View results in ShortCourse1.out

---> GEOCHEMICAL CONDITION: speciate1

Temperature (C)	=	25.000
Porosity	=	1.000
Liquid Saturation	=	1.000
Liquid Density (kg/m ³)	=	997.075
Solid Density (kg/m ³)	=	0.000
Solid:Solution Ratio	=	0.000
Ionic Strength	=	0.010
Solution pH	=	5.658
Total Charge	=	-1.735E-18

---> GEOCHEMICAL CONDITION: speciate3

Temperature (C)	=	25.000
Porosity	=	1.000
Liquid Saturation	=	1.000
Liquid Density (kg/m ³)	=	997.075
Solid Density (kg/m ³)	=	0.000
Solid:Solution Ratio	=	0.000
Ionic Strength	=	0.010
Solution pH	=	5.658
Total Charge	=	-1.735E-18

---> GEOCHEMICAL CONDITION: speciate2

Temperature (C)	=	25.000
Porosity	=	1.000
Liquid Saturation	=	1.000
Liquid Density (kg/m ³)	=	997.075
Solid Density (kg/m ³)	=	0.000
Solid:Solution Ratio	=	0.000
Ionic Strength	=	0.030
Solution pH	=	7.717
Total Charge	=	1.966E-02

Exercise 1: Carbonate Speciation with Isotopes

View results in ShortCourse1.out

```
*****
---> GEOCHEMICAL CONDITION: speciate1
Total Aqueous Concentrations of Primary Species
-----
```

Species	Molality	Constraint	Constraint Phase
H+	-6.4078E-19	Charge	
C02(aq)	1.3074E-05	Gas	C02(g)
13C02(aq)	1.3206E-07	Gas	13C02(g)
Ca++	1.0326E-30	Total	
Na+	1.0000E-02	Total	
Cl-	1.0000E-02	Total	

$\delta^{13}\text{C} = 0\text{‰}$

Concentrations of Individual Species, Exchangers, and Surface Complex

Species	Log Molality	Log Activity	Molality	Activity
H+	-5.619	-5.658	2.403E-06	2.197E-06
C02(aq)	-4.975	-4.974	1.060E-05	1.063E-05
13C02(aq)	-6.971	-6.970	1.070E-07	1.072E-07
Ca++	-29.987	-30.157	1.031E-30	6.968E-31
Na+	-2.001	-2.045	9.987E-03	9.009E-03
Cl-	-2.001	-2.047	9.987E-03	8.981E-03
HC03-	-5.612	-5.657	2.443E-06	2.204E-06
H13C03-	-7.606	-7.650	2.479E-08	2.236E-08

$\delta^{13}\text{C} = 4.6\text{‰}$

Speciation in ShortCourse1.out

From Speciate1

Concentrations of Individual Species, Exchangers, and Surface Complexes

Species	Log Molality	Log Activity	Molality	Activity	Activity Coefficient	Type
H+	-5.619	-5.658	2.403E-06	2.197E-06	9.141E-01	Aqueous
CO2(aq)	-4.975	-4.974	1.060E-05	1.063E-05	1.002E+00	Aqueous
13CO2(aq)	-6.971	-6.970	1.070E-07	1.072E-07	1.002E+00	Aqueous
Ca++	-29.987	-30.157	1.031E-30	6.969E-31	6.758E-01	Aqueous
Na+	-2.001	-2.045	9.987E-03	9.009E-03	9.022E-01	Aqueous
Cl-	-2.001	-2.047	9.987E-03	8.981E-03	8.994E-01	Aqueous
HCO3-	-5.612	-5.657	2.443E-06	2.204E-06	9.022E-01	Aqueous
H13CO3-	-7.606	-7.650	2.479E-08	2.236E-08	9.022E-01	Aqueous
CaCl+	-32.859	-32.904	1.383E-33	1.248E-33	9.022E-01	Aqueous
CaCl2(aq)	-34.905	-34.904	1.246E-35	1.249E-35	1.002E+00	Aqueous
CaOH+	-37.304	-37.349	4.967E-38	4.481E-38	9.022E-01	Aqueous
HCl(aq)	-7.006	-7.005	9.864E-08	9.887E-08	1.002E+00	Aqueous
NaCl(aq)	-4.875	-4.874	1.333E-05	1.336E-05	1.002E+00	Aqueous
NaOH(aq)	-11.187	-11.186	6.506E-12	6.521E-12	1.002E+00	Aqueous
OH-	-8.287	-8.333	5.158E-09	4.646E-09	9.008E-01	Aqueous
CO3--	-10.146	-10.323	7.146E-11	4.749E-11	6.645E-01	Aqueous
13CO3--	-12.140	-12.317	7.250E-13	4.817E-13	6.645E-01	Aqueous
CaCO3(aq)	-37.165	-37.164	6.836E-38	6.852E-38	1.002E+00	Aqueous
Ca13CO3(aq)	-39.159	-39.158	6.937E-40	6.953E-40	1.002E+00	Aqueous
CaHCO3+	-34.726	-34.771	1.879E-35	1.695E-35	9.022E-01	Aqueous

***** Partial pressure of gases (bars) *****

CO2(g) 3.12000000E-04
13CO2(g) 3.15000000E-06

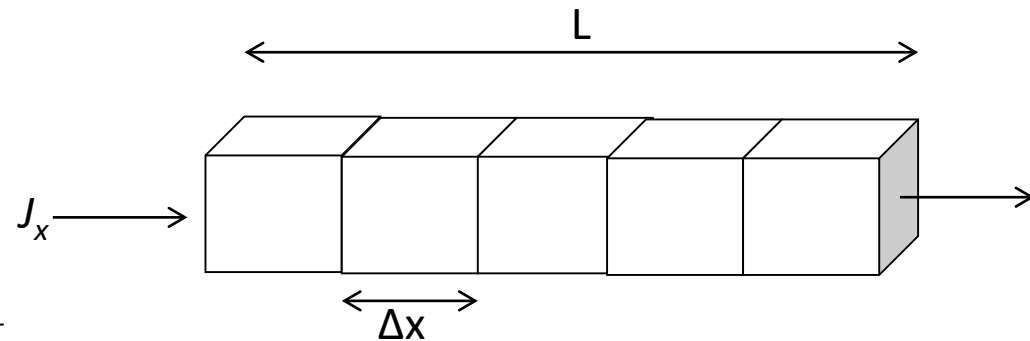
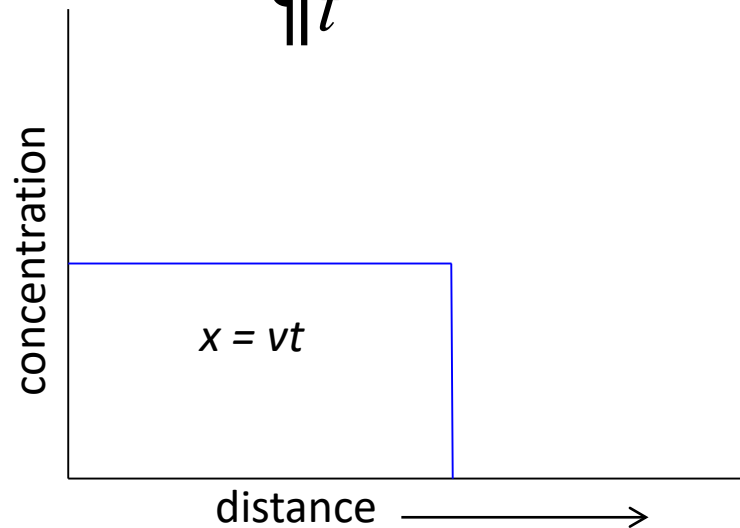
***** Saturation state of minerals (log[Q/K] *****

Calcite -32.0097

ADVECTION

Exercise 2: Advective Transport

$$\frac{\partial C}{\partial t} = - \tilde{N} \cdot [vC] = - v \frac{\partial C}{\partial x} \quad \leftarrow \text{For constant velocity and 1D}$$



Initial condition: junk2
 Left boundary: junk1 flux
 Right boundary: junk2 flux

$$CFL = \frac{v \Delta t}{\Delta x}$$

Courant-Friedrichs-Lewy Condition

Numerical Dispersion

$$\frac{C_i^{n+1} - C_i^n}{Dt} = -v \frac{C_i^n - C_{i-1}^n}{Dx}$$

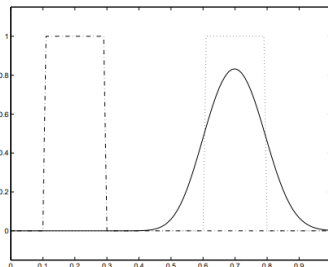
Upwind Scheme

$$C_i^{n+1} = C_i^n - Dt \frac{\partial C}{\partial t} + \frac{(Dt)^2}{2} \frac{\partial^2 C}{\partial t^2} + \dots$$

Taylor Series Expansions

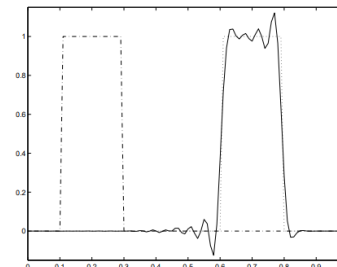
$$C_i^{n+1} = C_i^n - Dx \frac{\partial C}{\partial x} + \frac{(Dx)^2}{2} \frac{\partial^2 C}{\partial x^2} + \dots$$

Even terms result in smearing and amplitude errors Odd terms result in oscillatory phase errors



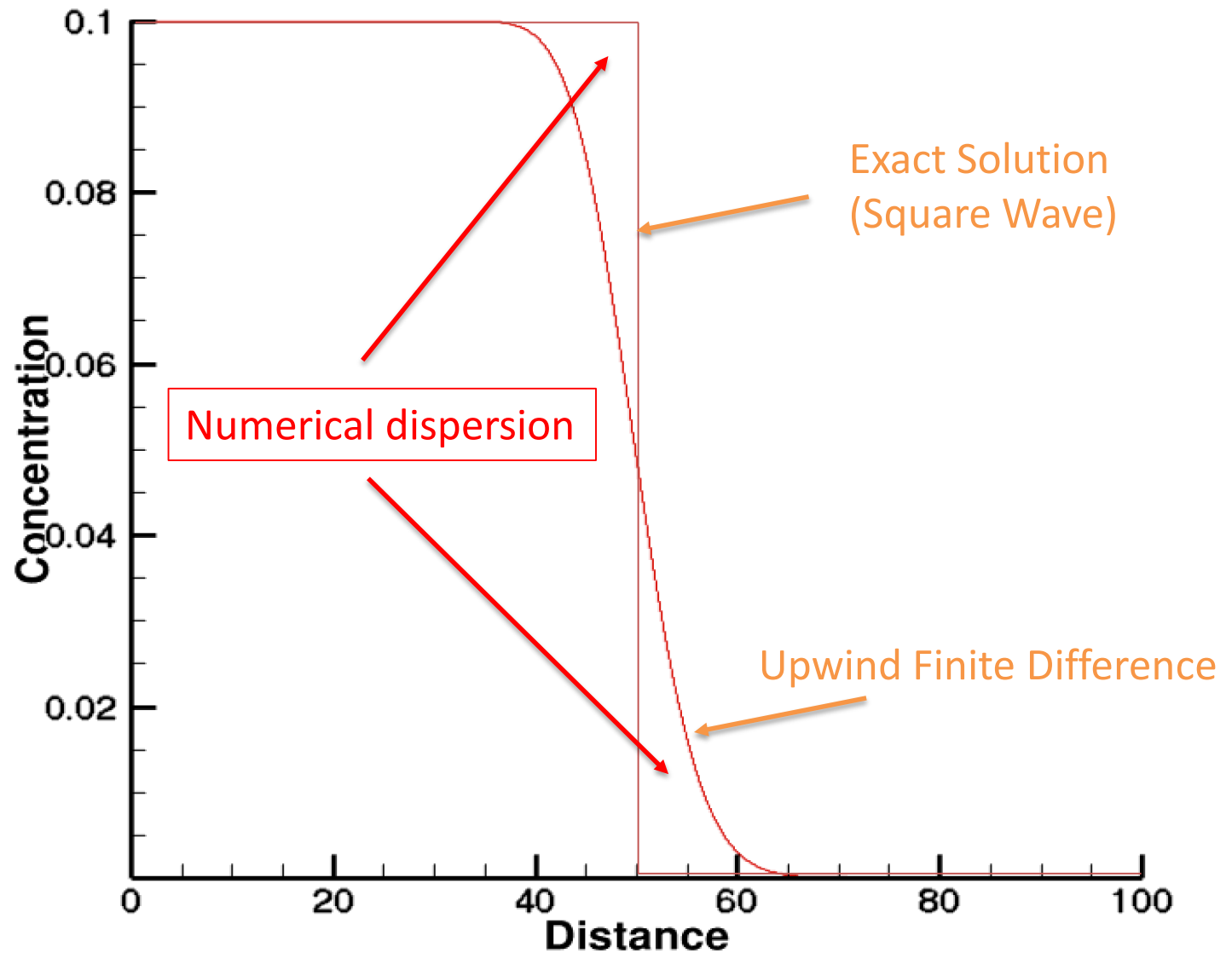
smearing (amplitude errors)

$$\frac{\partial u}{\partial t} + v \frac{\partial u}{\partial x} = 0$$



wiggles (phase errors)

Numerical Dispersion



Exercise 2 Procedure

1. Run CrunchTope in “GIMRT” mode, which uses 1st order upwind that introduces numerical dispersion

```
RUNTIME
time_units    years
timestep_max  0.010
timestep_init 0.010
time_tolerance 0.1
hindmarsh     true
master        Tracer
database_sweep no
speciate_only false
gimrt        true
database      datacom.dbs
END
```

```
FLOW
time_units    years
distance_units meters
constant_flow 1.0
END
```

```
TRANSPORT
distance_units meters
time_units    years
fix_diffusion 0.0
dispersivity 0.0
END
```

```
BOUNDARY_CONDITIONS
x_begin junk1 flux
x_end   junk2 flux
END
```

```
INITIAL_CONDITIONS
junk2 1-100
END
```

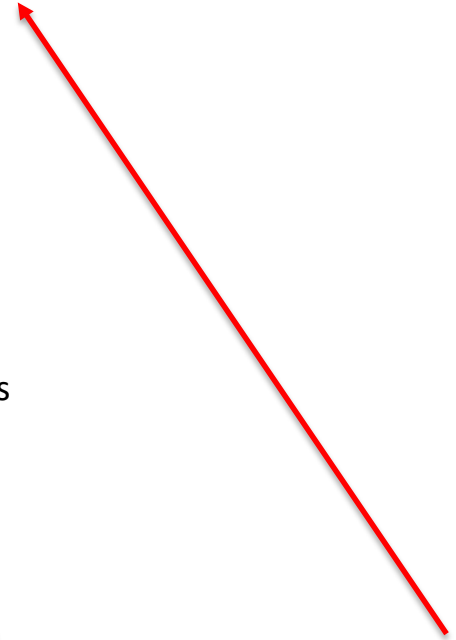
```
DISCRETIZATION
distance_units meters
xzones 100 1.00
END
```

```
Condition junk1
units      mol/kg
temperature 25.0
Tracer    0.1
END
```

```
Condition junk2
units      mol/kg
temperature 25.0
Tracer    0.000001
END
```

Boundary Condition

Initial Condition



Exercise 2 Procedure

1. Run CrunchTope in “GIMRT” mode, which uses 1st order upwind that introduces numerical dispersion
2. Save “totcon1.out” as “totcon1_gimrt.out” to avoid being written over
3. Change to “gimrt false” so as to use TVD 3rd order accurate scheme with van Leer limiters
4. Rerun and compare “totcon1_gimrt.out” with “totcon1.out”
5. Now gradually increase dispersion in the input file (while still using OS3D mode (“gimrt false”)) until you get a match between TVD (OS3D) profile and Upwind (GIMRT) profile

```
RUNTIME
time_units  years
timestep_max  0.010
timestep_init  0.010
time_tolerance  0.1
hindmarsh  true
master  Tracer
database_sweep  no
speciate_only  false
gimrt  false
database  datacom.dbs
END
```

Turns off upwinding, turns on higher order TVD scheme

```
TRANSPORT
distance_units  meters
time_units  years
fix_diffusion  0.0
dispersivity  0.01
END
```

$\propto v$

Units of meters

Gradually increase until you have a match

What dispersivity do you need to match?

FICKIAN DIFFUSION

Exercise 3: Fickian Diffusion



(a) early

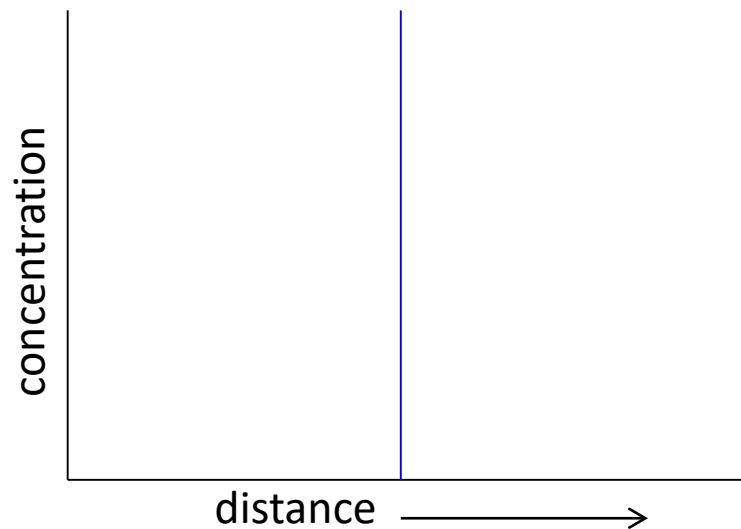


(b) intermediate



(c) late

Initial Condition



$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2}$$

Exercise 3: Fickian Diffusion

```
TRANSPORT
distance_units meters
time_units second
fix_diffusion 1.E-09
dispersivity 0.0
END
```

```
DISCRETIZATION
xzones 501 0.0002
END
```

```
INITIAL_CONDITIONS
initial 1-501
boundary 251-251
END
```

Writes over earlier
specified initial
condition

```
BOUNDARY_CONDITIONS
x_begin initial flux
x_end initial flux
END
```

“flux” uses flow rate
through boundary, if
flow rate = 0, then it
becomes a No Flux BC

```
FLOW
time_units years
distance_units meters
constant_flow 0.0
END
```

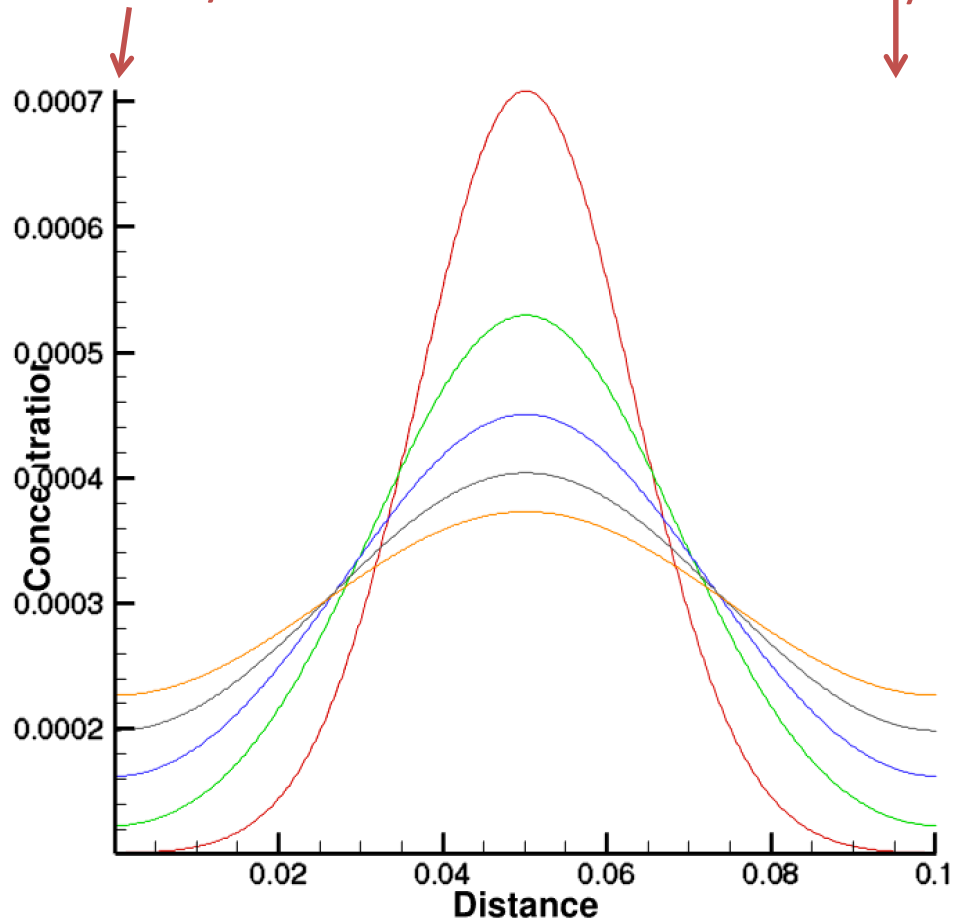
```
Condition boundary
units mol/kg
temperature 25.0
Tracer 0.1
END
Condition initial
units mol/kg
temperature 25.0
Tracer 0.0001
END
```

After running “flux” BC, switch to
“Dirichlet” (fixed concentration) and
compare results

```
BOUNDARY_CONDITIONS
x_begin initial Dirichlet
x_end initial Dirichlet
END
```

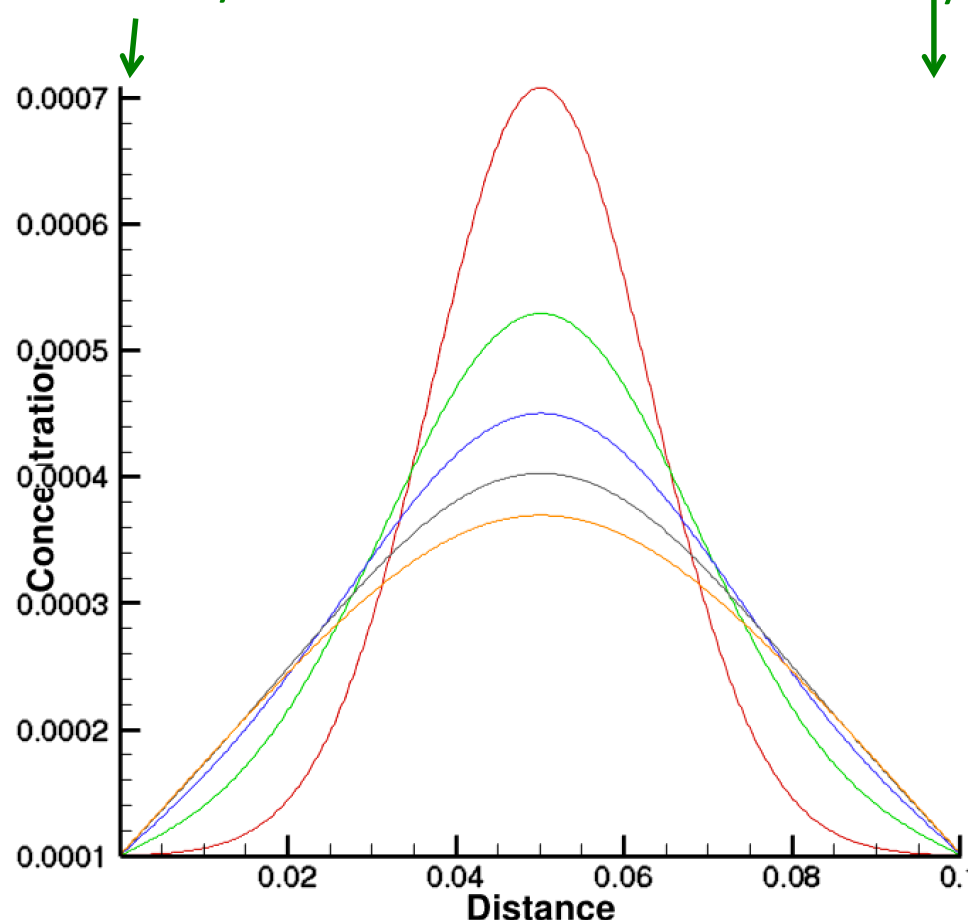
Exercise 3: Fickian Diffusion

Flux
boundary



Flux
boundary

Dirichlet
boundary



Dirichlet
boundary

NOTE: Error function analytical (ERF) solution only applies to infinite (or semi-infinite) boundary conditions, so would fail to describe system once mass reaches the boundary

NERNST-PLANCK MULTICOMPONENT DIFFUSION

Exercise 4: Multicomponent Diffusion

Flux from chemical potential

$$J_i = L_{ij} \nabla \mu_i$$

Fickian

**Electrical
Potential**

**Activity
Coefficient**

Nernst-Planck Equation

$$J_i = -D_i \nabla C_i - \frac{z_i F D_i C_i}{RT} \nabla \psi - D_i C_i \nabla \ln \gamma_i$$

Diffusion Potential

$$\nabla \psi = -\frac{RT}{F} \frac{\sum_j z_j D_j [\nabla C_j + C_j \nabla \ln \gamma_j]}{\sum_j z_j^2 D_j C_j}$$

Term vanishes if diffusion coefficients are all the same

CrunchTope Equation

$$J_i = -D_i [\nabla C_i] + z_i D_i C_i \frac{\sum_j z_j D_j [\nabla C_j]}{\sum_j z_j^2 D_j C_j}$$

Fick's Law

Diffusion Potential

Exercise 4: Multicomponent Diffusion (with Nernst-Planck Equation)

```

BOUNDARY_CONDITIONS
X_begin inlet      Dirichlet
X_end  initial    flux
END

TRANSPORT
distance_units centimeters
time_units seconds
fix_diffusion 1.000e-05
formation_factor 1.0
cementation_exponent 1.0
D_25 H+      9.312e-05
D_25 Na+     1.334e-05
D_25 Cl-     2.032E-05
D_25 OH-     5.26e-05
D_25 NO3-    1.00e-05
END
  
```

Refers to Condition "inlet" and "initial"

Species-specific diffusion coefficients

```

Condition initial
temperature 25.0
pH          4.0
Cl-         1.e-04
Na+         1.e-04
NO3-        1.e-04
CO2(aq)     CO2(g) 1.0E-16
END
  
```

```

Condition inlet
temperature 25.0
pH          6.0
Cl-         1.e-04
Na+         1.e-04
NO3-        1.e-06
CO2(aq)     CO2(g) 1.0E-16
END
  
```

NOTE: Hydrogen ion will try to diffuse faster than Cl⁻ and Na⁺

Change diffusion coefficients all to same number and compare results

```

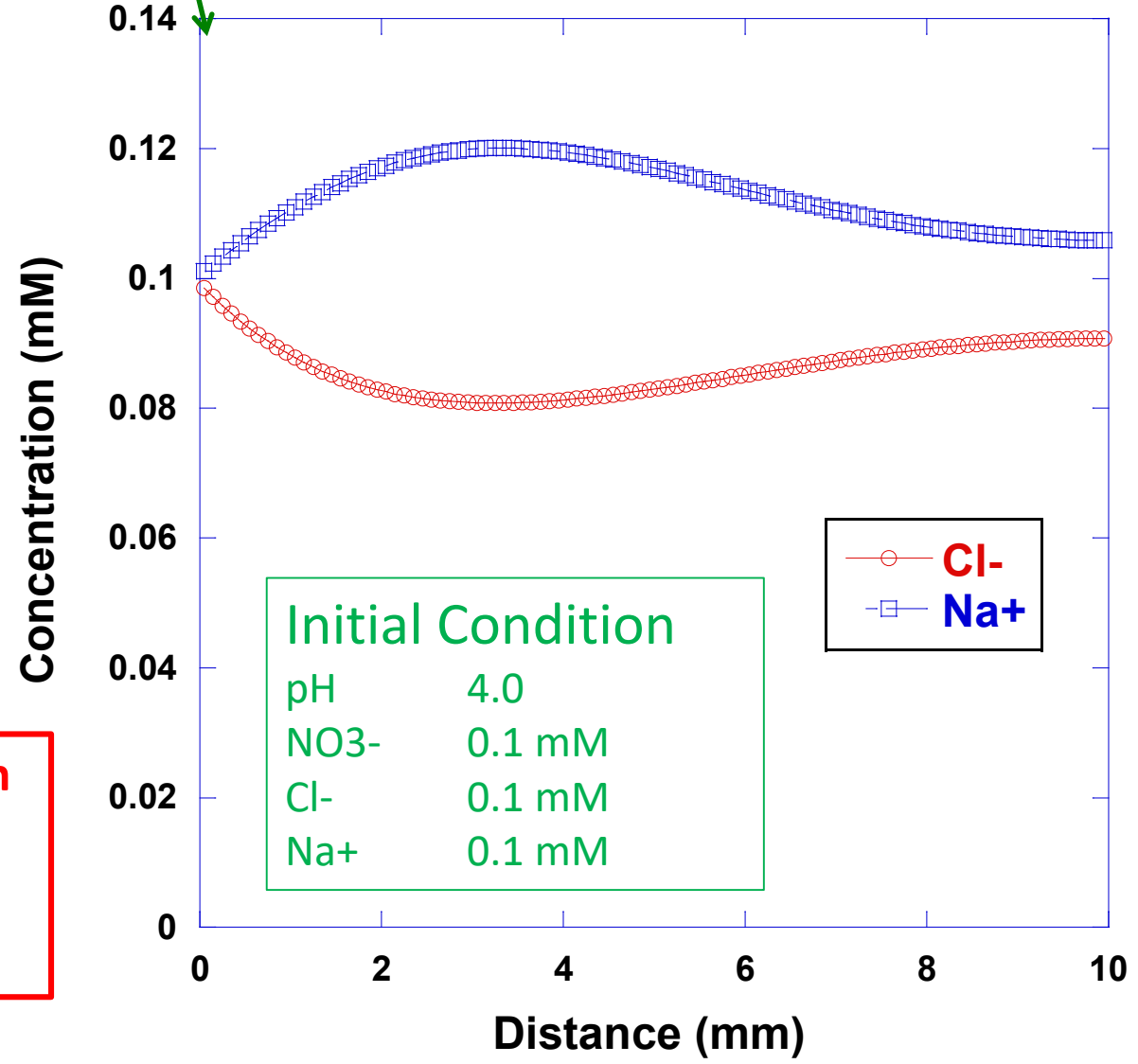
TRANSPORT
D_25 H+      1.000e-05
D_25 Na+     1.000e-05
D_25 Cl-     1.000e-05
D_25 OH-     1.000e-05
D_25 NO3-    1.000e-05
END
  
```


Exercise 4: Nernst-Planck Equation

Exercise 4

Left Boundary
pH 6.0
NO₃⁻ 0.001 mM
Cl⁻ 0.1 mM
Na⁺ 0.1 mM

NOTE: No initial gradient in Na⁺ or Cl⁻, so Fick's Law would say there is no diffusion



Initial Condition
pH 4.0
NO₃⁻ 0.1 mM
Cl⁻ 0.1 mM
Na⁺ 0.1 mM

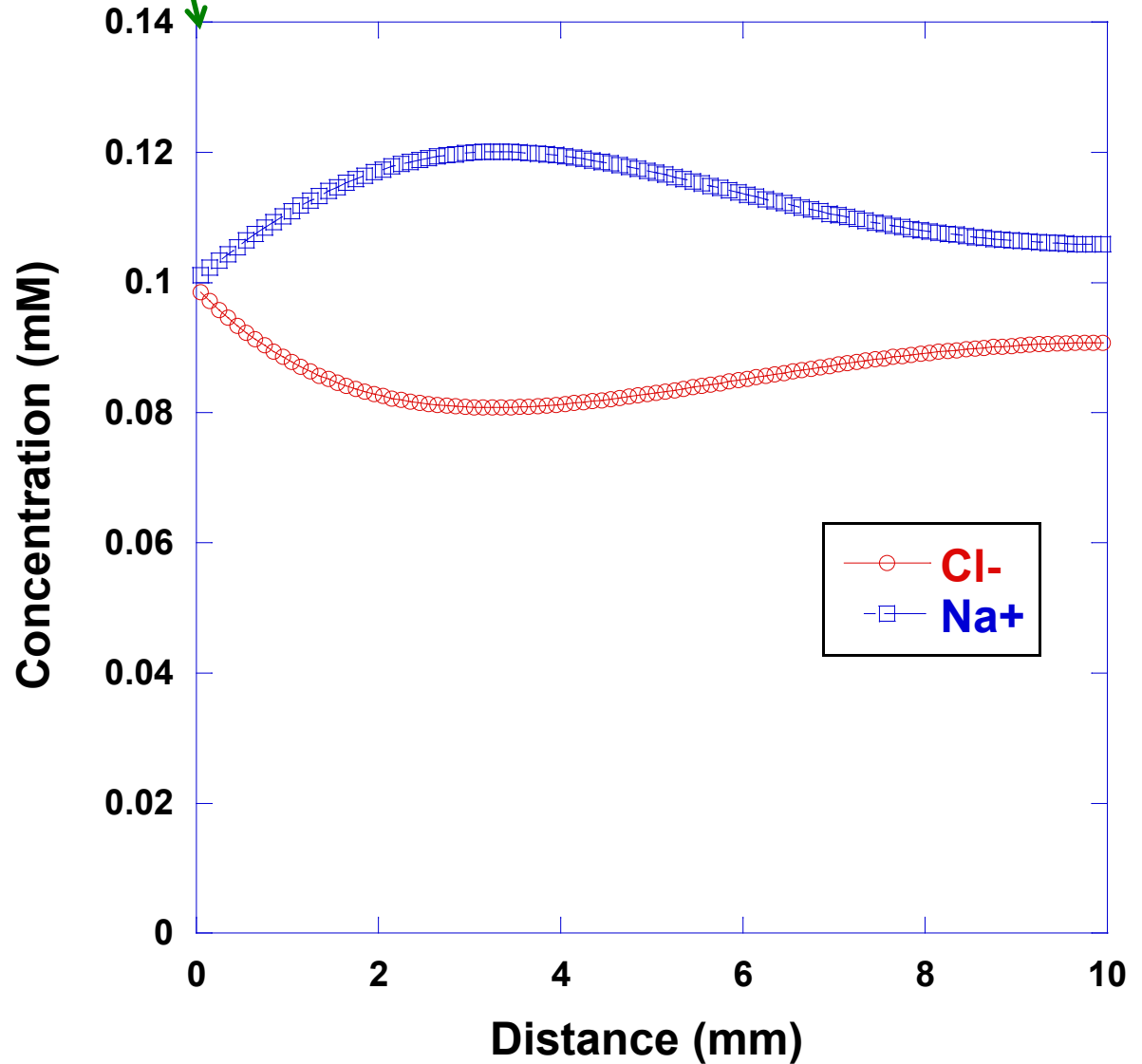
Exercise 4

Left Boundary

pH	6.0
NO ₃ ⁻	0.001 mM
Cl ⁻	0.1 mM
Na ⁺	0.1 mM

Initial Condition

pH	4.0
NO ₃ ⁻	0.1 mM
Cl ⁻	0.1 mM
Na ⁺	0.1 mM



Exercise 4: Nernst-Planck with $\delta^{37}\text{Cl}$

ISOTOPES

primary 37Cl- Cl- 0.333

END

Rare
Isotope

Common
Isotope

TRANSPORT

distance_units centimeters

time_units seconds

fix_diffusion 1.000e-05

formation_factor 1.0

cementation_exponent 1.0

D_25 H+ 9.312e-05

D_25 Na+ 1.334e-05

D_25 Cl- 2.032E-05

D_25 37Cl- 2.028E-05

D_25 OH- 5.26e-05

D_25 NO3- 1.00e-05

END

Isotopic fractionation
expressed in per mil

$$\delta = \left[\frac{\left[\frac{^{37}\text{Cl}}{^{36}\text{Cl}} \right]_{\text{sample}}}{\left[\frac{^{37}\text{Cl}}{^{36}\text{Cl}} \right]_{\text{std}}} - 1 \right] \cdot 1000$$

Isotope ratio of standard

Note difference in diffusion coefficients
(source of fractionation)

Find isotopic ratios in **tooperatio_aq1.out**

Exercise 4: Nernst-Planck with $\delta^{37}\text{Cl}$

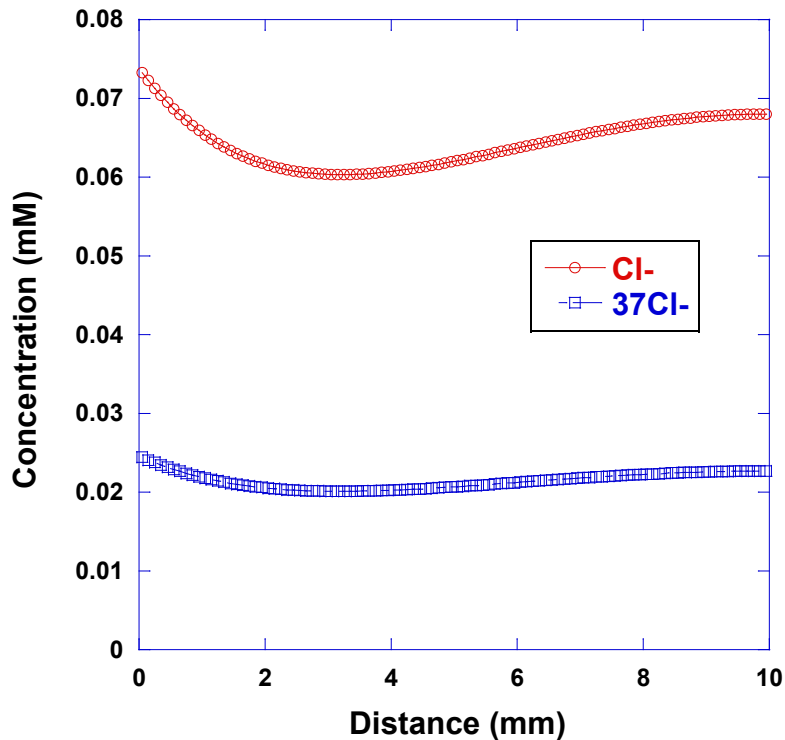
Left Boundary

pH	6.0
Cl-	0.075
^{37}Cl -	0.025
Na+	0.1
NO_3^-	0.001

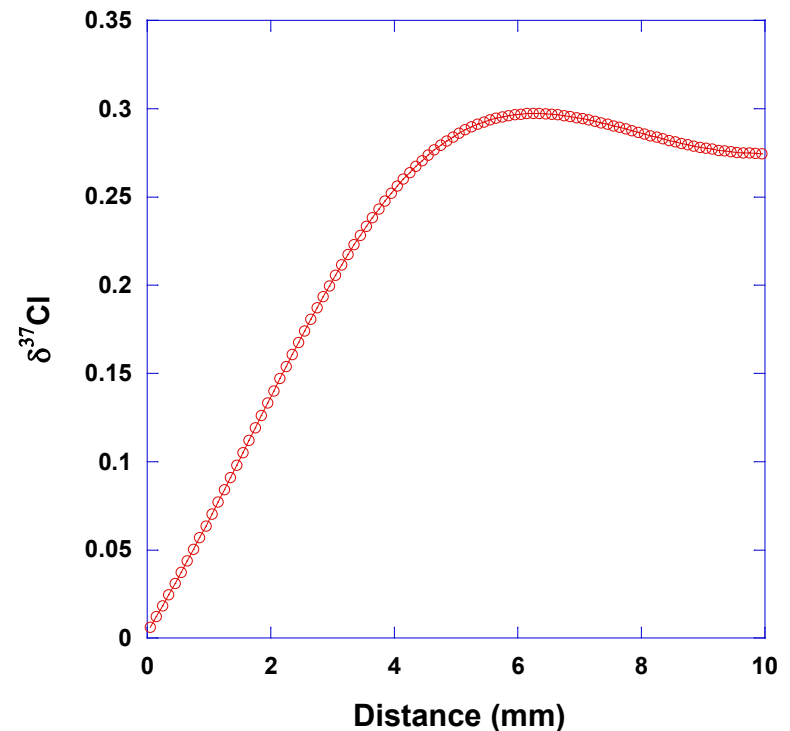
D_25	Cl-	2.032E-5
D_25	^{37}Cl -	2.028E-5

$$\delta = \left[\frac{\left[\frac{^{37}\text{Cl}}{^{36}\text{Cl}} \right]_{\text{sample}}}{\left[\frac{^{37}\text{Cl}}{^{36}\text{Cl}} \right]_{\text{std}}} - 1 \right] \cdot 1000$$

Exercise 4 Cl Isotopes



Isotope Fractionation



Plot isotopic ratios in `toperatio_aq1.out`

SORPTION

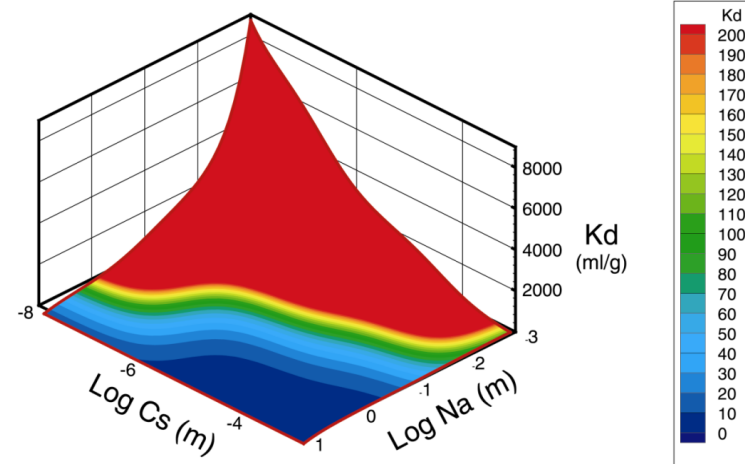
Contaminant Retardation

$$R = 1 + \frac{\rho_B K_d}{\phi}$$

ρ_B : bulk density (g/ml)

K_d : distribution coefficient (ml/g)

ϕ : porosity



$$R \frac{\partial C}{\partial t} = \frac{\partial}{\partial x_i} \left[D_{ij} \frac{\partial C}{\partial x_j} \right] - \frac{\partial}{\partial x_i} [v_i C]$$

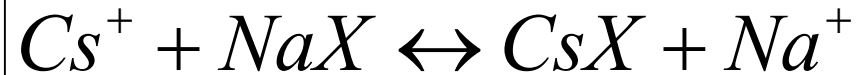
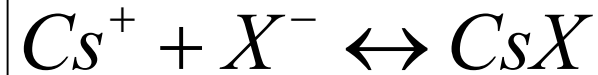
Contaminant

Velocity v_c

$$v_c = \frac{v_x}{R}$$

Exercise 6a: Cesium Ion Exchange

Exchange reaction involving Cs^+ and a competing Na^+



Gaines-Thomas convention for activity of an exchange species

$$\beta(i)_M = \frac{z_M q(i)_M}{\sum_M z_M q(i)_M}$$

Cation charge Moles/g

Single exchange site

$$CEC = \sum_M z_M q_M$$

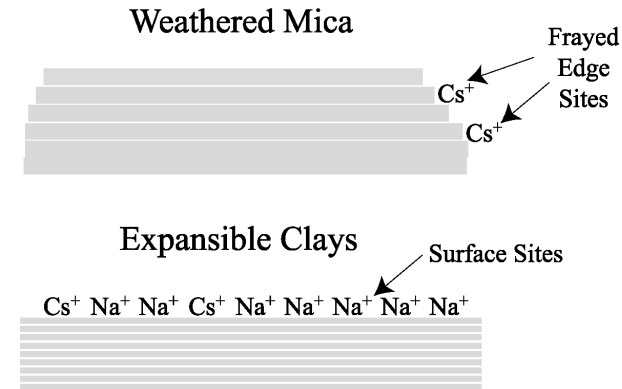
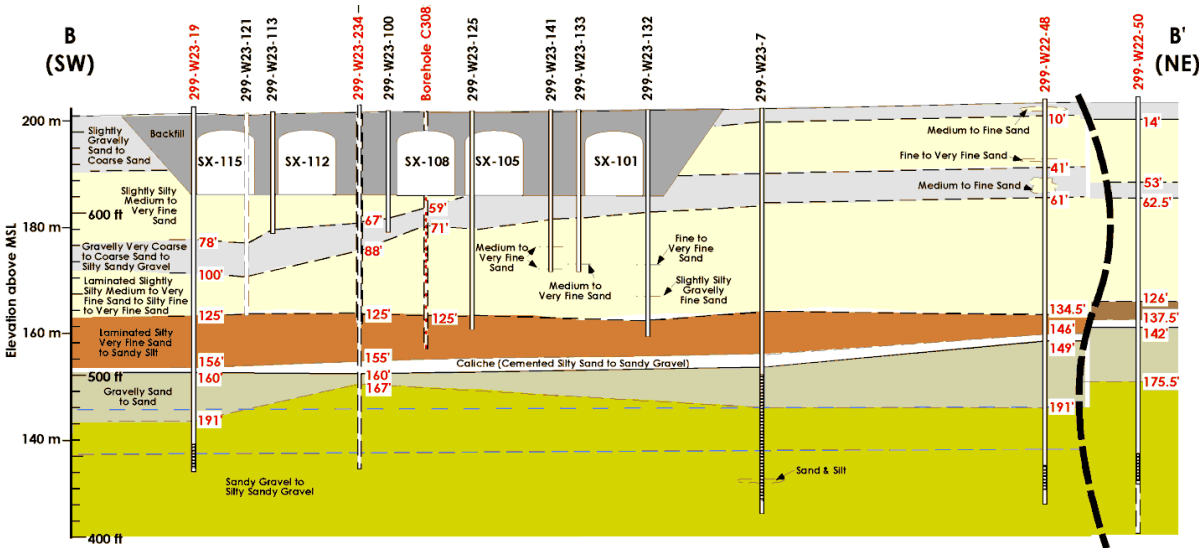
Multiple exchange sites

$$CEC = \sum_i \sum_M z_M q(i)_M$$

Cation Exchange Capacity:

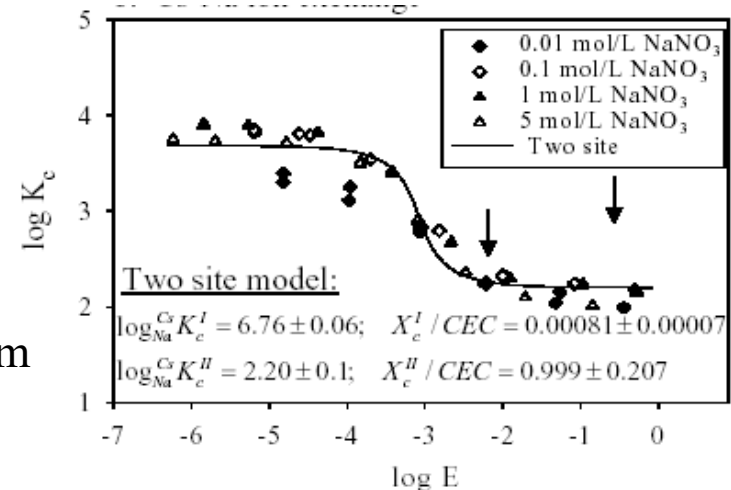
Real World Example for ^{137}Cs Cation Exchange

Leaking high ionic strength waste tanks led to contamination of the deep Hanford Vadose Zone



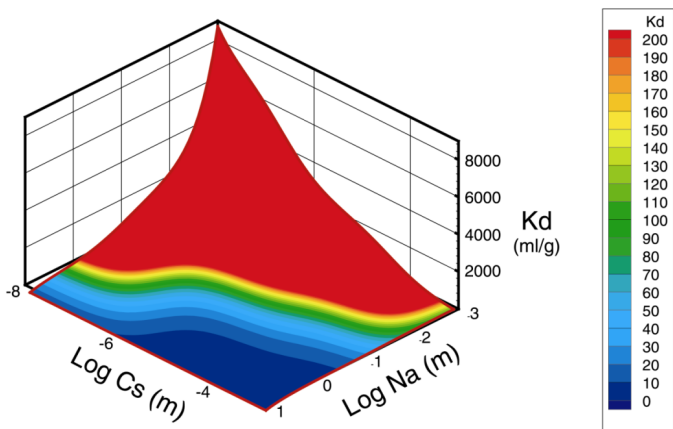
Failure of K_d models spawned a major Science and Technology Program at Hanford funded by the U.S. DOE

Binary exchange data from Zachara et al. (2002)



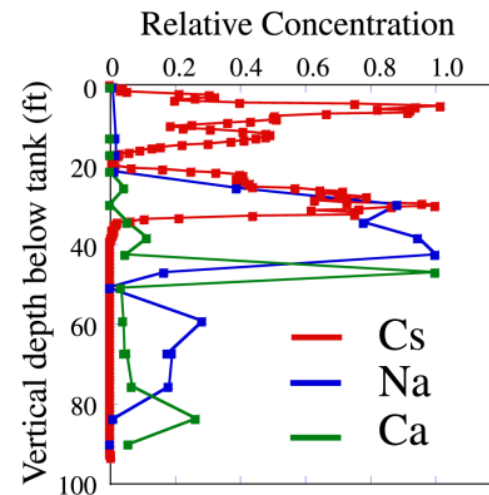
Cs Mobility in High Ionic Strength Solutions

Greatest mobility of ^{137}Cs was below the Hanford SX-108 tank



Cesium K_d in Hanford Sediments

Steefel et al., 2003;
2005

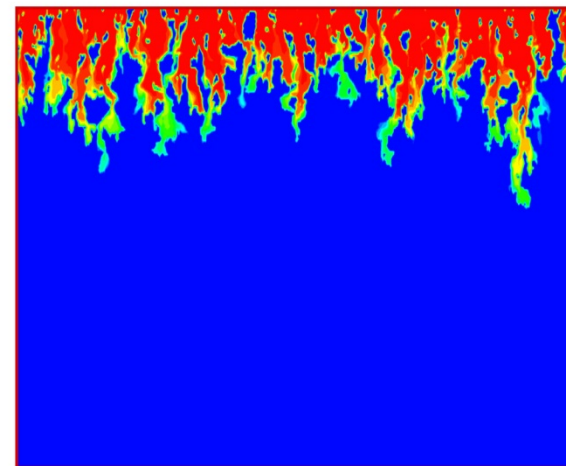
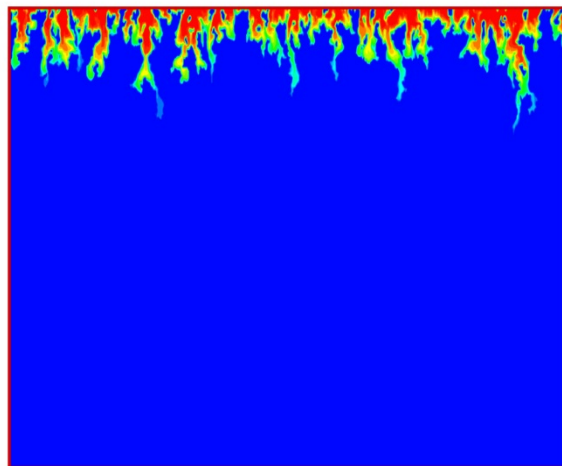
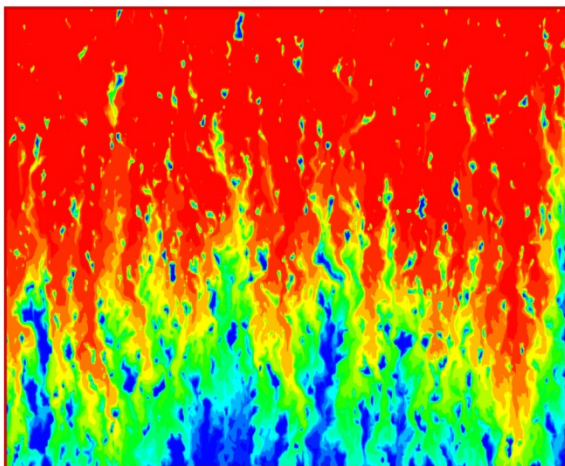


Nitrate

Cesium
(1M NaNO_3)

Cesium
(5M NaNO_3)

Relative Distance



Exercise 6a: Cesium Ion Exchange

Simulated sequence:

Input file	HanfordTank-A	HanfordTank-B	HanfordTank-C
NaNO ₃ injectate concentration	5 M	5 M	5 M
CsI injectate concentration	0	0.1 mM	0
Duration	19.25 hrs	125 hrs	76.5 hrs
Purpose	Precondition sediment	Active exchange of Cs for Na	Flushing sediment

Exercise 6a: Cesium Ion Exchange

```
RUNTIME
density_module  sodium_nitrate
database        HanfordTanksColumnFit3Site-GT.dbs
save_restart    Column3NaNO3Flush1.rst
later_inputfiles HanfordTank-B.in HanfordTank-C.in
END
```

```
OUTPUT
time_units      hours
spatial_profile 19.25
time_series      Expt3ColumnFit.out 100
time_series_print Cs+ I-
time_series_output 0.00
END
```

```
BOUNDARY_CONDITIONS
x_begin nano3flush      flux
x_end   initial_condition flux
END
```

```
POROSITY
fix_porosity 0.405
porosity_update false
END
```

```
ION_EXCHANGE
exchange Xhan1-
exchange Xhan2-
exchange Xhan3-
convention Gaines-Thomas
END
```

3 types of exchange sites

```
DISCRETIZATION
distance_units centimeters
xzones 100 0.15228
END
```

Database entries for log K (selectivity coefficients)
Assumes half-exchange reactions

Frayed edge site on illite

Planar sites on illite

```
Begin exchange
'NaXhan1' 2 1.0 'Na+' 1.0 'Xhan1-' 7.25224
'NaXhan2' 2 1.0 'Na+' 1.0 'Xhan2-' 4.93359
'NaXhan3' 2 1.0 'Na+' 1.0 'Xhan3-' 1.98868
'CsXhan1' 2 1.0 'Cs+' 1.0 'Xhan1-' 0.00
'CsXhan2' 2 1.0 'Cs+' 1.0 'Xhan2-' 0.00
'CsXhan3' 2 1.0 'Cs+' 1.0 'Xhan3-' 0.00
```

Exercise 6a: Cesium Ion Exchange

Initial Condition

```
Condition initial_condition
units          molar
temperature    25.0
pH             8.0
HCO3-         CO2(g) 3.15e-04
K+            0.0015
NO3-          0.001
Cs+          0.000
I-            0.000
Na+           0.001
Ca++          Calcite
Mg++          0.00005
Tracer        0.0
Cl-           charge
Xhan1- -cec  2.277023E-08
Xhan2- -cec  2.621486E-07
Xhan3- -cec  1.20E-04

Calcite       0.01  specific_surface_area 0.1
SolidDensity -ss_ratio 4698
END
```

Frayed edge
site on illite
(eq/g)

Planar sites
on illite (eq/g)

Sodium Nitrate Flush

```
Condition nano3flush
units          molar
temperature    25.0
pH             8.0
HCO3-         CO2(g) 3.15e-04
K+            1.e-5
Cs+          0.0
I-            0.0
Na+           1.00
NO3-          1.00
Ca++          0.0
Mg++          0.0
Tracer        0.001
Cl-           0.0
Xhan1- -cec  2.277023E-08
Xhan2- -cec  2.621486E-07
Xhan3- -cec  1.20E-04
Calcite       0.01  specific_surface_area 0.1
SolidDensity -ss_ratio 4698
END
```

```
BOUNDARY_CONDITIONS
x_begin nano3flush      flux
x_end   initial_condition flux
END
```

```
FLOW
time_units  years
distance_units meters
constant_flow 638.2
END
```

Exercise 6a: Cesium Ion Exchange

Cesium Spike: HanfordTank-B.in

Sodium Nitrate Flush: HanfordTank-C.in

```
Condition cesiumflush
units      molar
temperature 25.0
pH         8.0
HCO3-     CO2(g) 3.15e-04
K+        1.e-5
Cs+      1.05e-4
I-        1.05e-4
Na+       1.00
NO3-     1.00
Ca++     0.000
Mg++     0.0
Tracer   0.001
Cl-      0.0
Xhan1- -cec 2.277023E-08
Xhan2- -cec 2.621486E-07
Xhan3- -cec 1.20E-04
Calcite  0.01 specific_surface_area 0.1
SolidDensity -ss_ratio 4698
END
```

This run "inherits"
NaNO₃ exchanged
sediment from
HanfordTank-A run

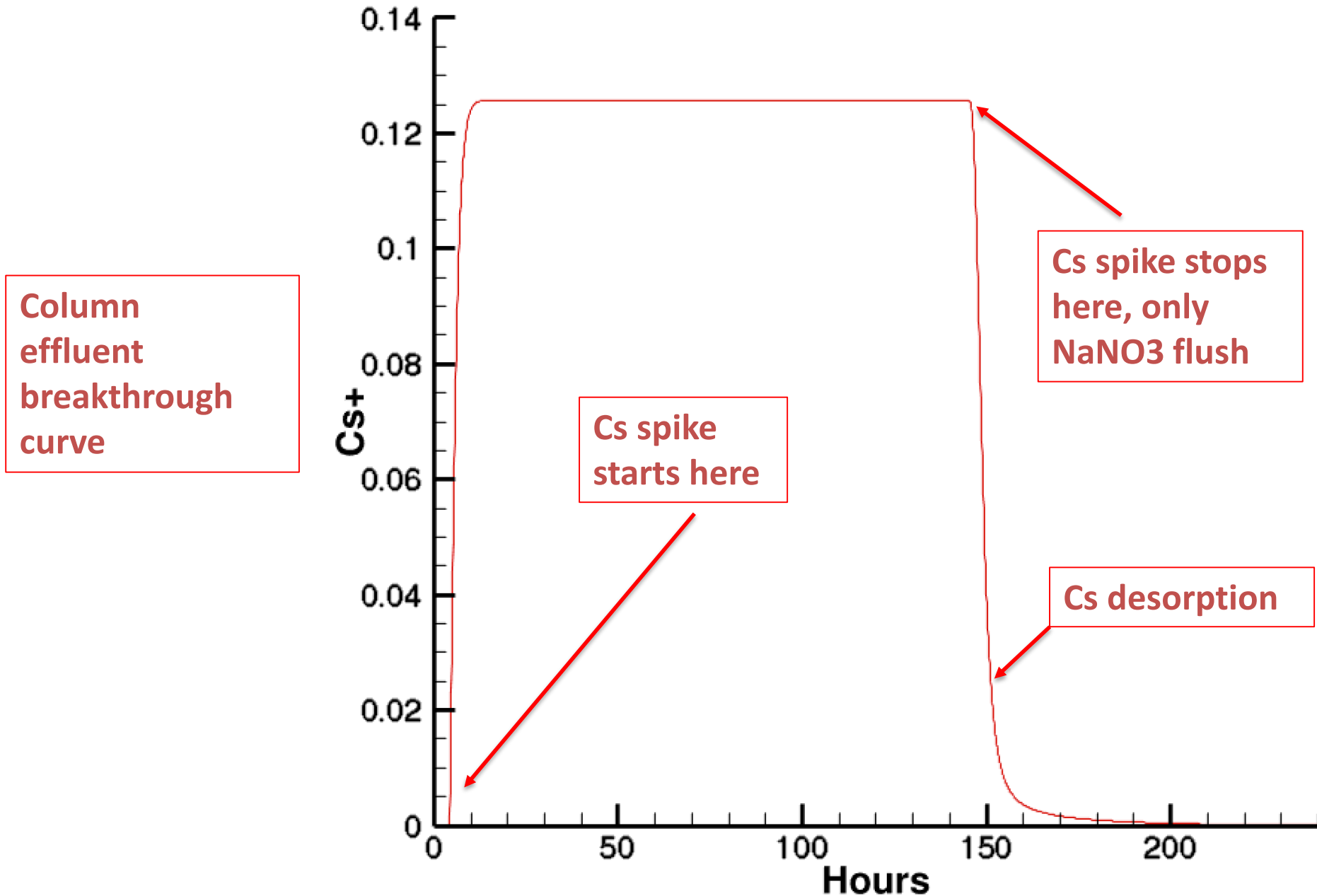
```
Condition nano3flush
units      molar
temperature 25.0
pH         8.0
HCO3-     CO2(g) 3.15e-04
K+        1.e-5
Cs+      0.0
I-        0.0
Na+       1.00
NO3-     1.00
Ca++     0.0
Mg++     0.0
Tracer   0.001
Cl-      0.0
Xhan1- -cec 2.277023E-08
Xhan2- -cec 2.621486E-07
Xhan3- -cec 1.20E-04
Calcite  0.01 specific_surface_area 0.1
SolidDensity -ss_ratio 4698
END
```

This run "inherits"
Cs contaminated
sediment from
HanfordTank-B run

```
BOUNDARY_CONDITIONS
x_begin cesiumflush flux
x_end   initial_condition flux
END
```

```
BOUNDARY_CONDITIONS
x_begin nano3flush flux
x_end   initial_condition flux
END
```

Exercise 6a: Cesium Ion Exchange



Exercise 6b: Surface Complexation

Protonation-deprotonation reactions controlling surface charge

Surface Hydroxyl



$$K_{a1} = \frac{[SOH^0][H^+]}{[SOH_2^+]}$$

First Acidity Constant



$$K_{a2} = \frac{[SO^-][H^+]}{[SOH^0]}$$

Second Acidity Constant

Electrostatic Effects

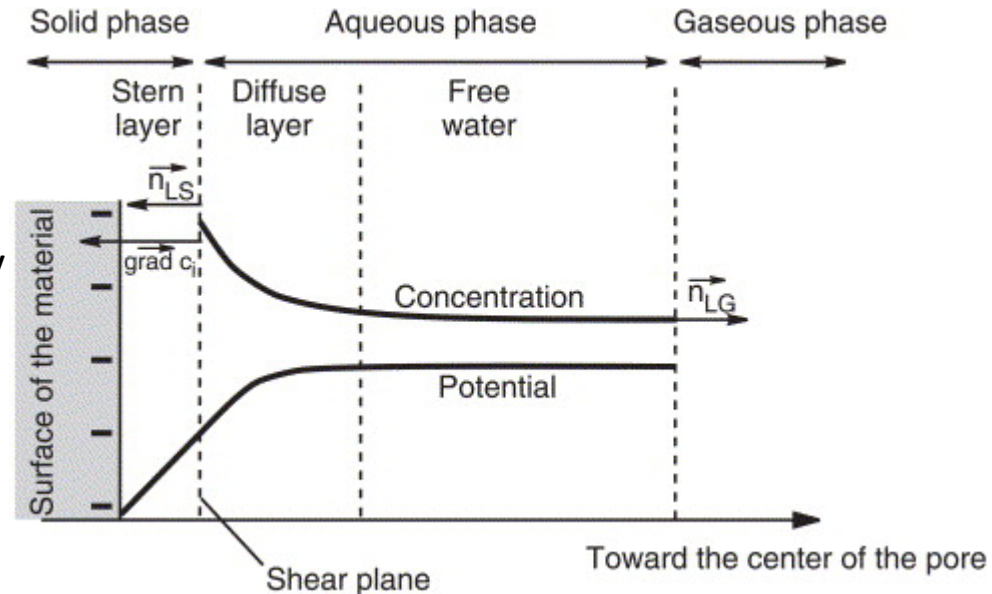
$$W = (+)_{\text{surface sites}} - (-)_{\text{surface sites}}$$

$$Q = W / \text{mass sorbent}$$

$$\sigma (C / m^2) = \frac{QF}{A} \leftarrow \text{Surface charge density}$$

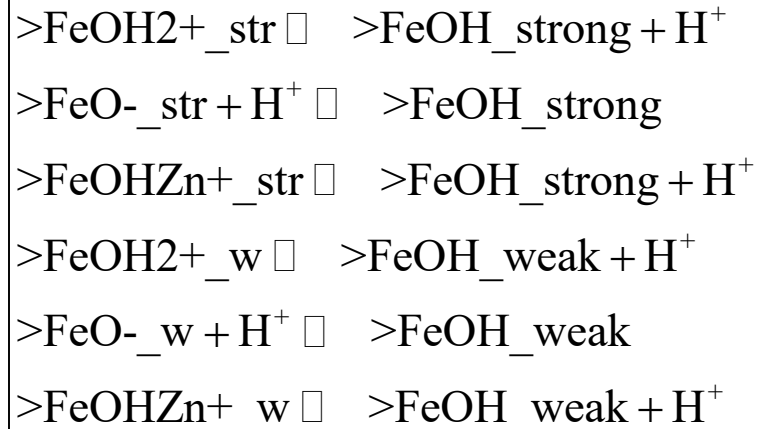
$$\Delta G_{ads} = \Delta G_{chem} + \Delta G_{coul}$$

$$K_a = K_{intrinsic} \exp \left[\frac{\Delta z F \Psi}{RT} \right]$$



Exercise 6b: Surface Complexation

Surface Complexation of Zn^{+2} on $Fe(OH)_3$



$$C_{sites} = \frac{\rho_{sites} A_{specific} MW_m \phi_m}{1000 V_m}$$

```

!!!Site name    <site density mol/m**2>
>FeOH_weak     3.703704E-06
>FeOH_strong   9.259259E-08
Fe(OH)3        2.943109E-05  specific_surface_area 600.0
!!! Note: Gives 0.09 g/kgw water Fe(OH)3, 54 m**2 surface
    
```

Exercise will “sweep” the pH from 5.0 to 8.0 to show the Zn “pH edge”

Exercise 6b: Surface Complexation

```
OUTPUT
time_units      days
spatial_profile 365
time_series_at_node PHREEQCexample8.out 1 1 1
```

```
SURFACE_COMPLEXATION
>FeOH_strong on Fe(OH)3
>FeOH_weak   on Fe(OH)3
END
```

```
Condition Solution1
temperature      25.0
pH               5.00
Zn++             1.E-07      equilibrate_surface
Na+              charge
NO3-             1.0000E-01
Fe+++            0.00
O2(aq)           2.4647E-04
!Site name      <site density mol/m**2>
>FeOH_weak      3.703704E-06
>FeOH_strong    9.259259E-08
Fe(OH)3         2.943109E-05 specific_surface_area 600.0
SolidDensity     2600.0
```

Partitions total concentration between surface and aqueous

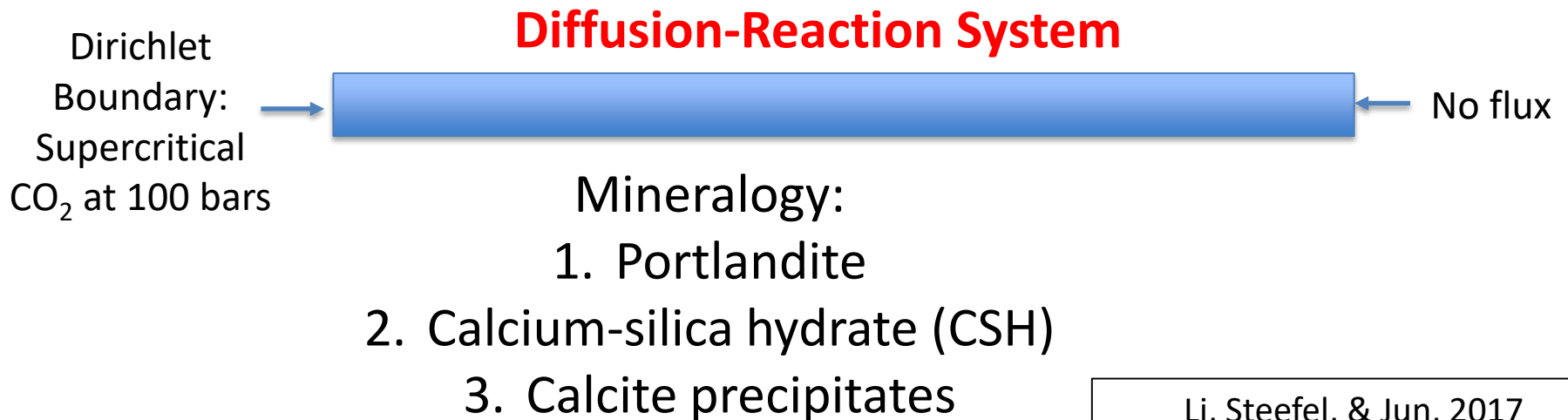
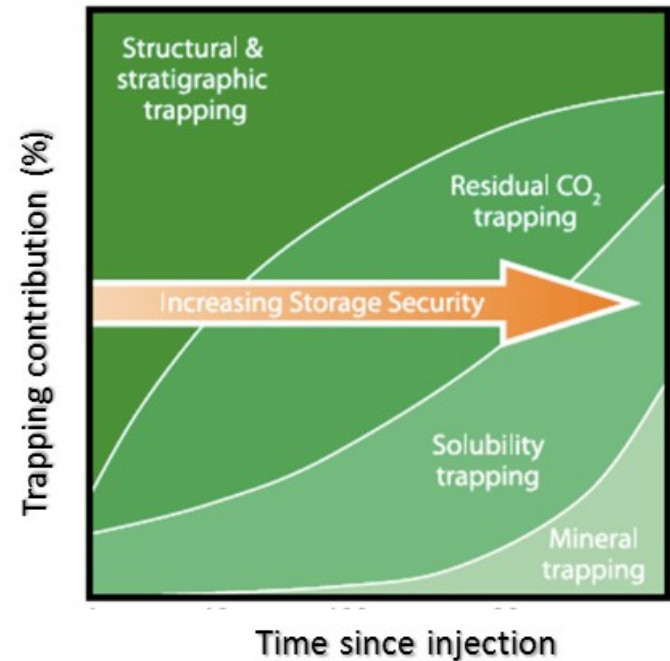
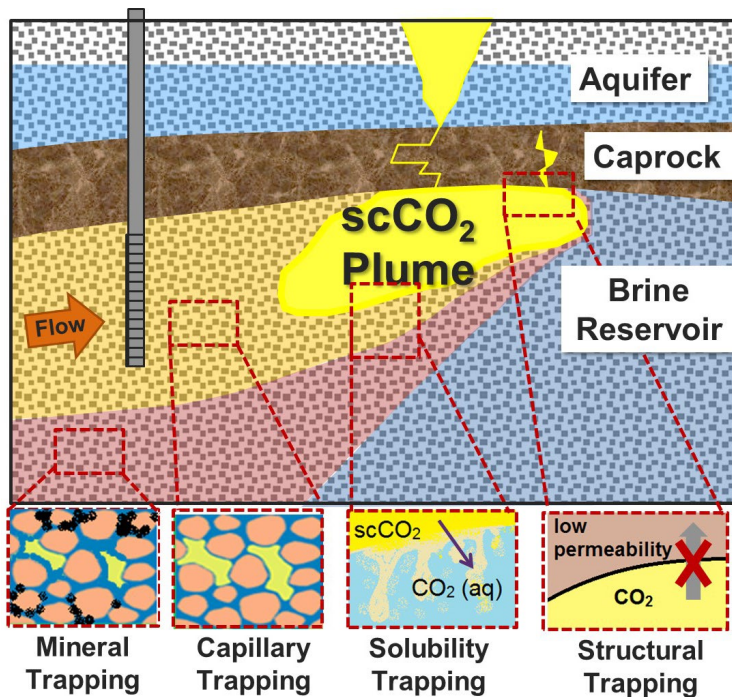
Site densities for weak and strong sites

!! Note: Gives 0.09 g/kgw water Fe(OH)₃, 54 m² surface
!! Based on a density of 1017 kg/m³, 1.017 g/cm³
!! Volume Fraction Fe(OH)₃ [m³/m³]*0.001*Molecular Weight Fe(OH)₃/(Porosity*Molar Volume Fe(OH)₃ [m³/mole]) = g/L, but we want g/kg water, so g/L * (1/ro) = g/kgw

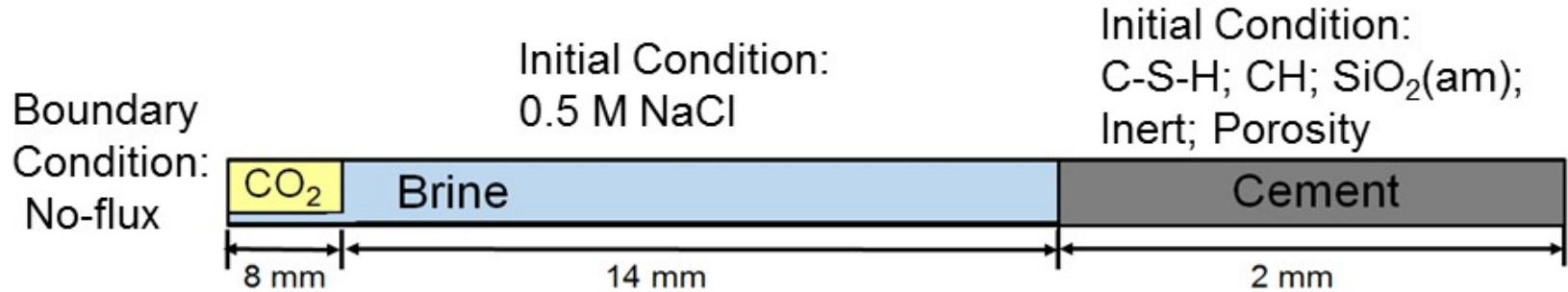
END

CO₂ ATTACK ON CEMENT

Exercise 7: CO₂ Attack on Cement



Exercise 7: CO₂ Attack on Cement

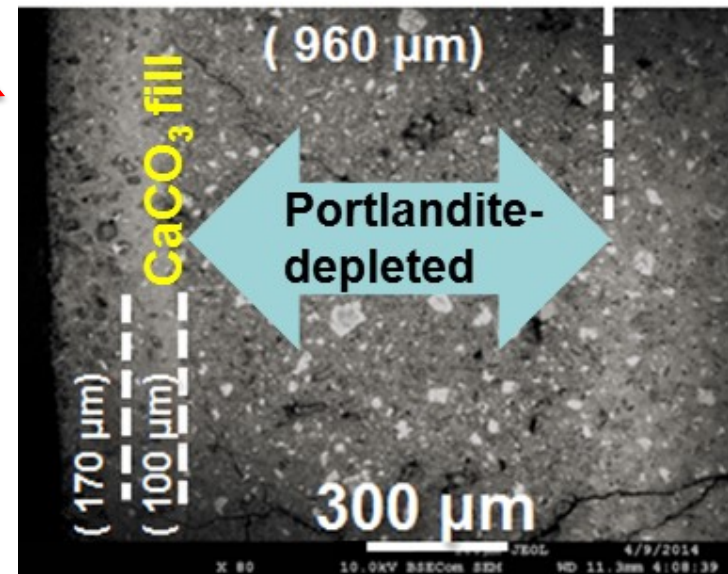


Super-critical CO₂

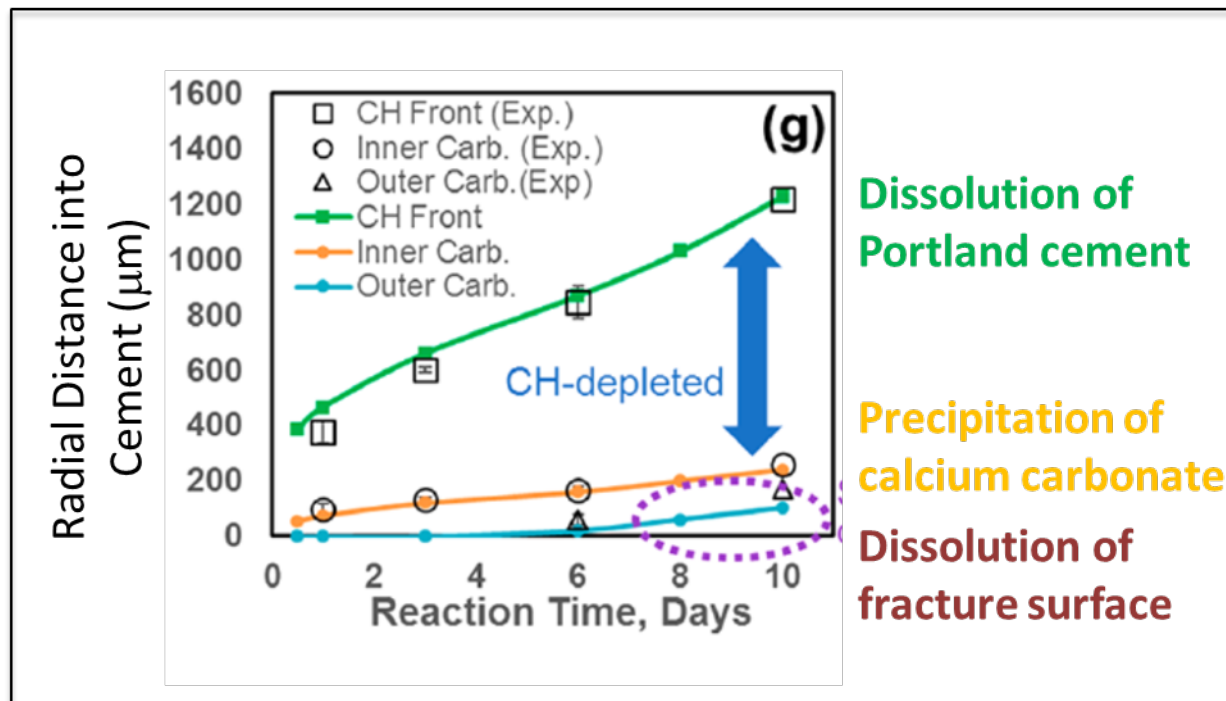
Cement

Based on:

Li, Q., C.I. Steefel, Y-S Jun (2017) Deciphering calcium carbonate precipitation associated with CO₂ attack on cement using reactive transport modeling. *Environmental Science and Technology* **51**: 10861-10871, doi: 10.1021/acs.est.7b00594.



Exercise 7: CO₂ Attack on Cement



Dissolution of Portland cement

Precipitation of calcium carbonate

Dissolution of fracture surface

Li, Q., C.I. Steefel, Y-S Jun (2017) Deciphering calcium carbonate precipitation associated with CO₂ attack on cement using reactive transport modeling. *Environmental Science and Technology* **51**: 10861-10871, doi: 10.1021/acs.est.7b00594.

Exercise 7: CO₂ Attack on Cement

```
RUNTIME
!!!fix_saturation 0.999
read_saturationfile QL_Saturation.dat
Duan      true
Qingyun  true
```

```
POROSITY
porosity_update true
minimum_porosity 0.015
porosity_exponent 3.00
porosity_threshold 0.017
END
```

```
Calcite      -label nucleatecalcite
Calcite      -label h+ -rate -3.0
Calcite_mix  -label h+ -rate -3.0
SiO2(ammix) -label default -rate -6.5
SiO2(am)     -label default -rate -6.5
SiO2(am)    -label nucleateSiO2(am)
Portlandite  -label default -rate -5.0
CSH(1.6)    -label default -rate -7.8
CSH(0.8)    -label default -rate -7.8
Bogusite     -rate -35.00
Bogusite_i   -rate -35.00
```

Two calcites with slightly different solubility

```
NUCLEATION
&Nucleation
NameMineral = Calcite
label       = nucleatecalcite
A_zero25C   = 0.00000001
B_nucleation = 0.000905
Sigma_mJm2  = 47
SSA_m2g     = 1
Surface     = Bogusite_i
/
END
NUCLEATION
&Nucleation
NameMineral = SiO2(am)
label       = nucleateSiO2(am)
A_zero25C   = 0.00000001
B_nucleation = 0.000905
Sigma_mJm2  = 20000
SSA_m2g     = 1
Surface     = Bogusite_i
/
END
```

Annotations:

- Pre-exponential J_0 (points to A_zero25C)
- Constant terms (points to B_nucleation)
- Interfacial free energy (points to Sigma_mJm2)
- Specific surface area of nucleated phase (points to SSA_m2g)
- Template for nucleation (points to Surface)

$$R_{precipitation} = J_0 \exp \left[-\frac{\sigma^3 \nu^2}{3k_B^3 T^3 (\ln \Omega)^2} \right] A_{quartz}$$

Exercise 7: CO₂ Attack on Cement

```
Condition Brine-Seed
!!Solution w/o minerals
temperature 95.0
units mol/kg
pH charge
CO2(aq) CO2(g) 100.0
Ca++ 0.0
SiO2(aq) 0.000001
SO4-- 0.0
Na+ 0.5
Cl- 0.50064
Calcite 0.0 ssa 1
Calcite_mix 0.0 ssa 1
SiO2(am) 0.0 ssa 1
SiO2(ammix) 0.0 ssa 1
CSH(1.6) 0.0
CSH(0.8) 0.0
Portlandite 0.0
Bogusite 0.0 0.0
Bogusite_i 0.01 ssa 1
set_porosity 16
!!set_saturation 0.95
```

```
DISCRETIZATION
distance_units microns
xzones 4 2000 320 100 200 10
END
```

```
Condition Cement
temperature 95.0
pH Portlandite
CO2(aq) 1.E-10
Ca++ 0.001
Na+ charge
Cl- 0.500
SiO2(aq) 0.0000001
Calcite_mix 0.00001 ssa 1
CSH(1.6) 0.31 ssa 1
CSH(0.8) 0.05 ssa 1
SiO2(ammix) 0.01 ssa 1
Portlandite 0.16 ssa 1
Bogusite 0.27 0.0
set_porosity 0.20
!!set_saturation 1
END
```

```
INITIAL_CONDITIONS
Brine 1-324
CO2 1-4
Brine-Seed 210-310
Cement 325-524
END
```

Li et al, 2017

Exercise 7: CO₂ Attack on Cement

Reactive Surface Area Options

```
Condition Cement
temperature      95.0
pH               Portlandite
CO2(aq)         1.E-10
Ca++            0.001
Na+             charge
Cl-             0.500
SiO2(aq)        0.0000001
Calcite         0.00001      ssa 1
CSH(1.6)       0.35       ssa 1
SiO2(am)       0.10       ssa 1
Portlandite    0.20       ssa 0.01
Bogusite       0.20       1.0
Teflon         0.0        1.0
set_porosity   0.15
END
```

Specific Surface Area (m²/g)

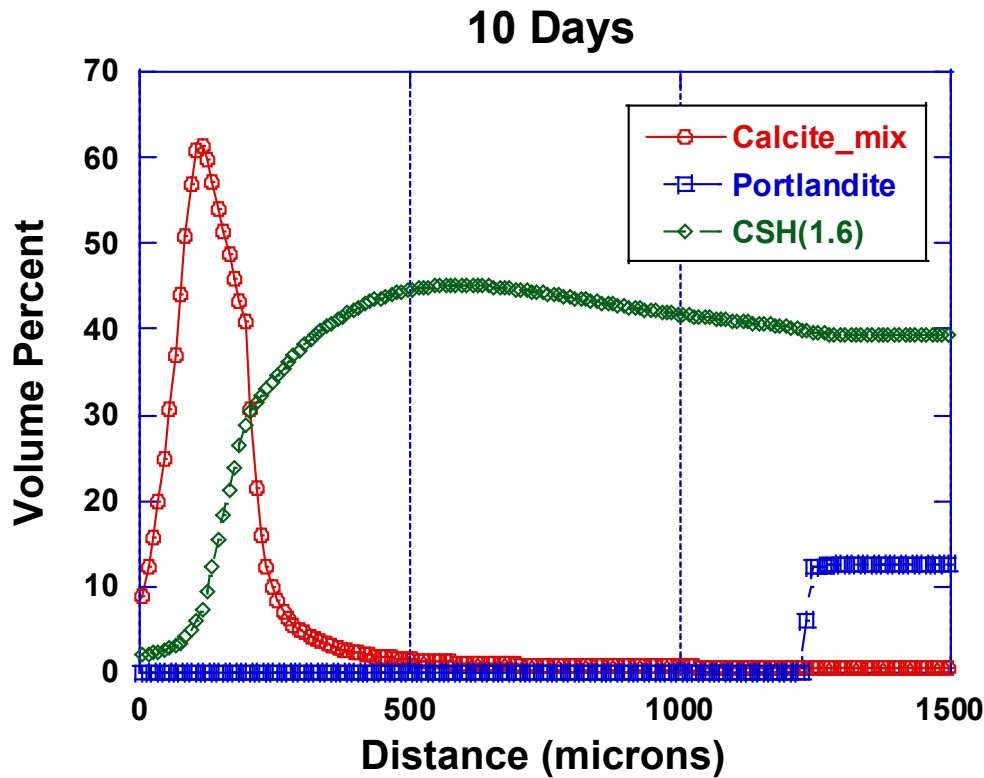
Bulk Surface Area (m²/m³)

```
1.0000000e-01
1.0000000e-01
1.0000000e-01
1.0000000e-01
1.0000000e+00
1.0000000e+00
```

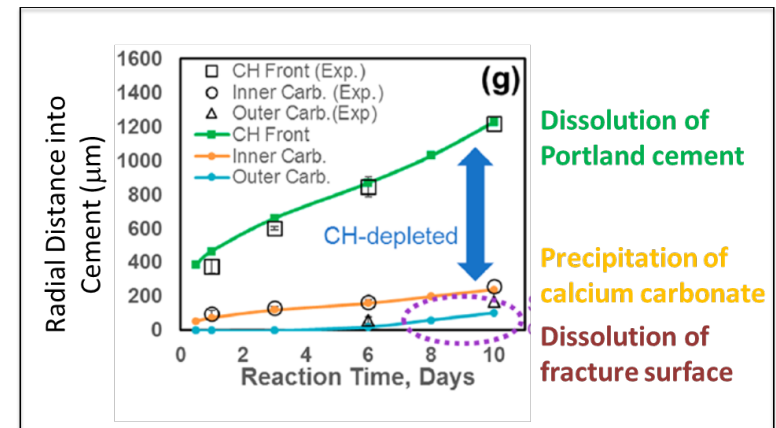
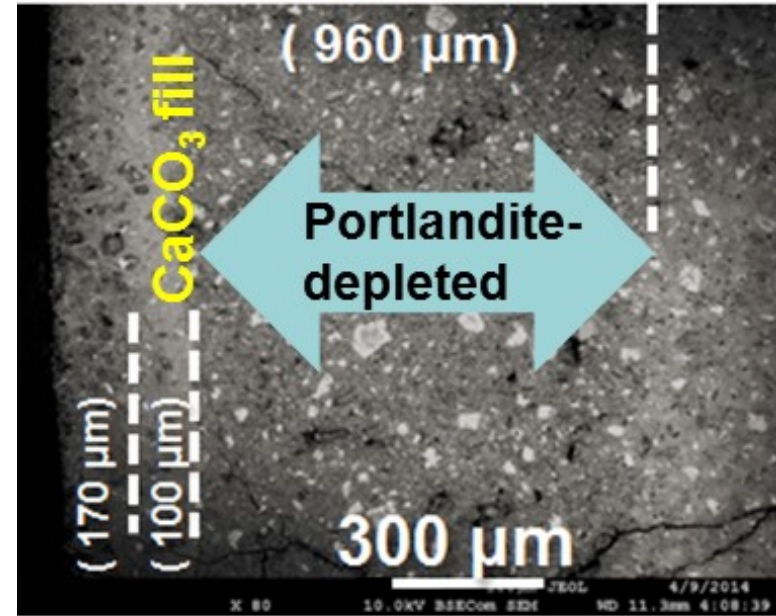
1st four grid cells are unsaturated (10%)

```
RUNTIME
time_units  days
!!fix_saturation 0.999
read_saturationfile QL-saturation.dat
```


Exercise 7: CO₂ Attack on Cement

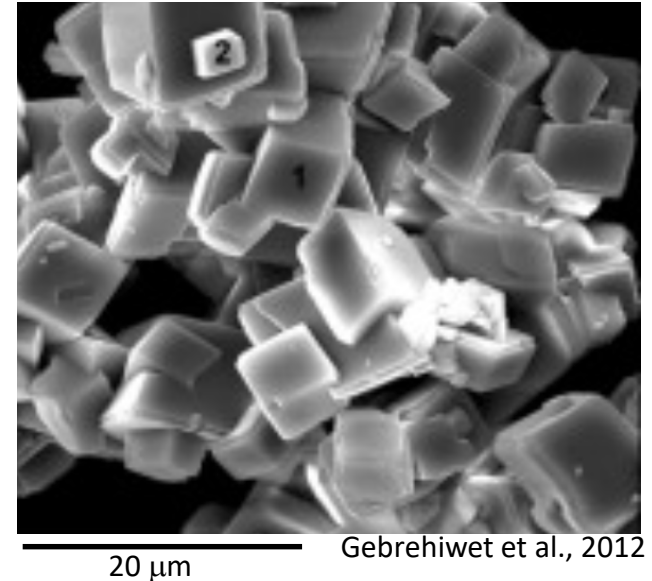
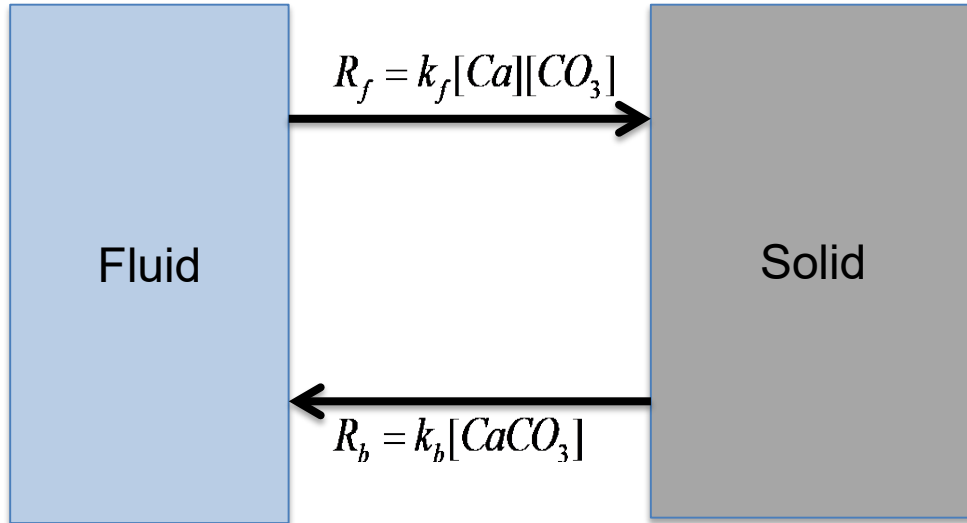


Li et al, ES&T, 2017



ISOTOPIC FRACTIONATION

Exercise 8: Calcite precipitation with $\delta^{44}\text{Ca}$



$$R_{net} = R_f - R_b = k_f[\text{Ca}][\text{CO}_3] - k_b[\text{CaCO}_{3(s)}]$$

$$R_{net} = [\text{CaCO}_{3(s)}]k \left[\frac{[\text{Ca}^{2+}][\text{CO}_3^{2-}]}{[\text{CaCO}_{3(s)}]} \frac{1}{K_{eq}} - 1 \right]$$

At equilibrium, $R_{net} = 0$

$$R_f = R_b$$

$$k_f[\text{Ca}^{2+}][\text{CO}_3^{2-}] = k_b[\text{CaCO}_{3(s)}]$$

$$\frac{k_b}{k_f} = \frac{[\text{Ca}^{2+}][\text{CO}_3^{2-}]}{[\text{CaCO}_{3(s)}]} = K_{eq}$$

Exercise 8: Calcite precipitation with $\delta^{44}\text{Ca}$

Isotope activities based on mole fractions

$${}^{44}X = \frac{[{}^{44}\text{CaCO}_3]}{[\text{CaCO}_3]}$$

$$R_{net} = [\text{CaCO}_{3(s)}] k \left[\frac{[\text{Ca}^{2+}][\text{CO}_3^{2-}]}{[\text{CaCO}_{3(s)}]} \frac{1}{K_{eq}} - 1 \right]$$
$$[{}^{40}\text{CaCO}_3] + [{}^{44}\text{CaCO}_3] = [\text{CaCO}_3]$$

$${}^{40}R_N = {}^{40}k_b {}^{40}X \left(\frac{[{}^{40}\text{Ca}][\text{CO}_3]}{K_{sp} {}^{40}X} - 1 \right)$$

$${}^{44}R_N = {}^{44}k_b {}^{44}X \left(\frac{[{}^{44}\text{Ca}][\text{CO}_3]}{K_{sp} {}^{44}X} - 1 \right)$$

Exercise 8: Calcite precipitation with $\delta^{44}\text{Ca}$

INITIAL_CONDITIONS

```
amendment 1-1  
END
```

DISCRETIZATION

```
distance_units centimeters  
xzones 1 1.0  
END
```

```
condition amendment  
units mmol/kg  
temperature 25.0  
H+ 0.11544  
Ca++ 5.28  
Ca44++ 0.111997921  
HCO3- 10.0  
!! Mineral name <volume fraction m3/m3>  
CalciteRifle 0.7833831 bsa 1.33E-02  
Calcite44Rifle 0.0166170 bsa 1.33E-02  
END
```

MINERALS

```
CalciteRifle -label default -rate -4.10000000  
!!! 2 per mil kinetic fractionation Kinetic fractionation  
Calcite44Rifle -label default -rate -4.10217692  
END
```

ISOTOPES

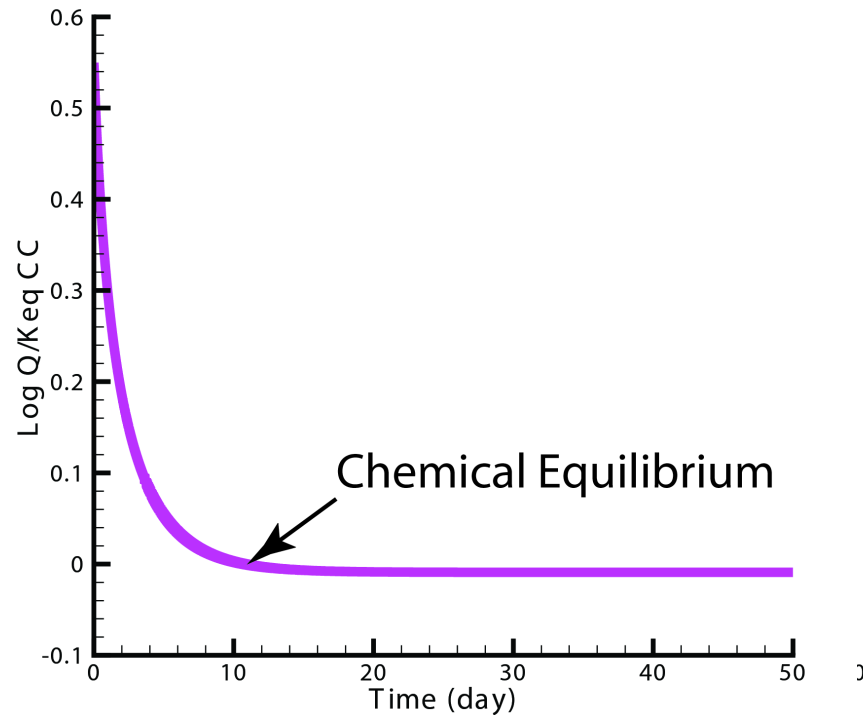
```
primary Ca44++ Ca++ Isotope Standard 0.021667  
mineral Calcite44Rifle CalciteRifle bulk  
isotope_time_series BatchExperiment.out 1 1  
1  
END
```

Isotopic back-reaction with

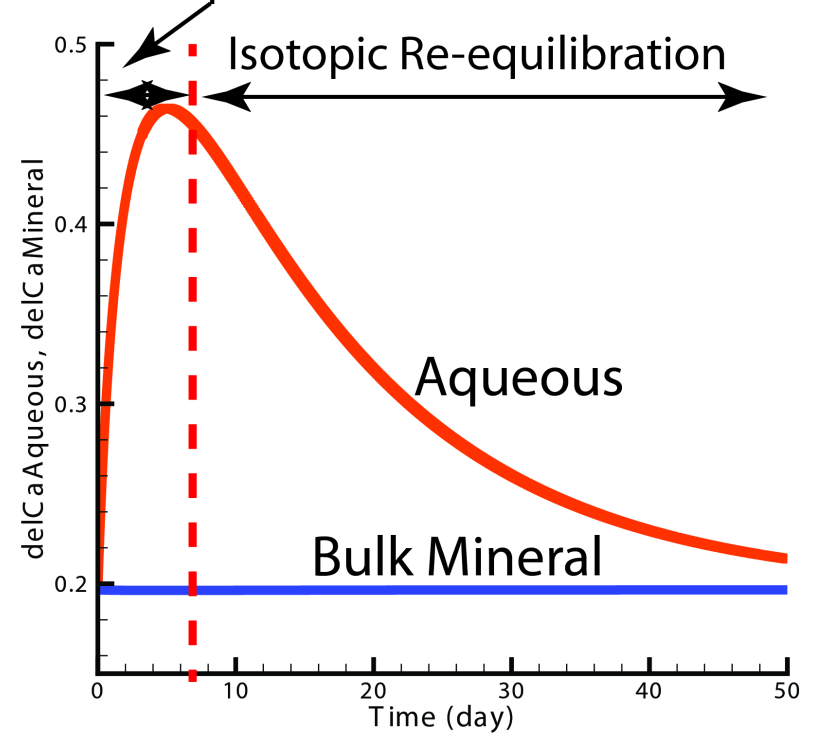
- Bulk
- Surface
- None

Output isotope time series to file at grid cell

Exercise 8: Calcite precipitation with $\delta^{44}\text{Ca}$



Kinetic Fractionation
due to Precipitation

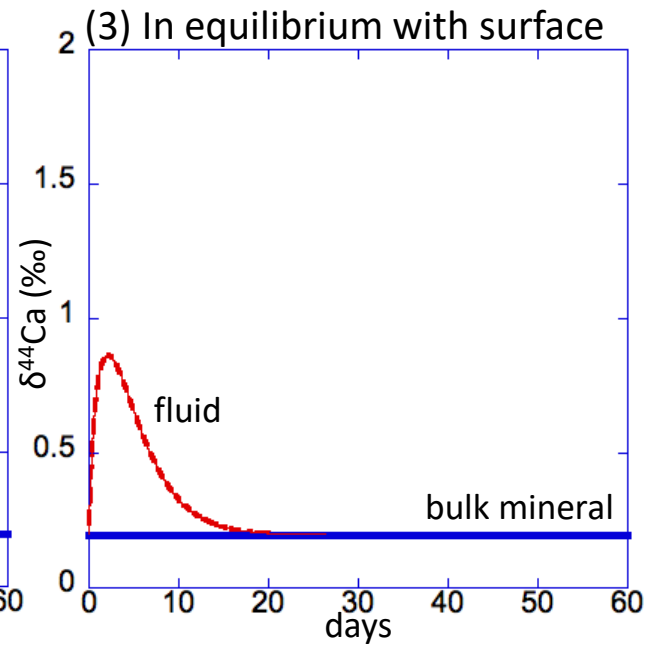
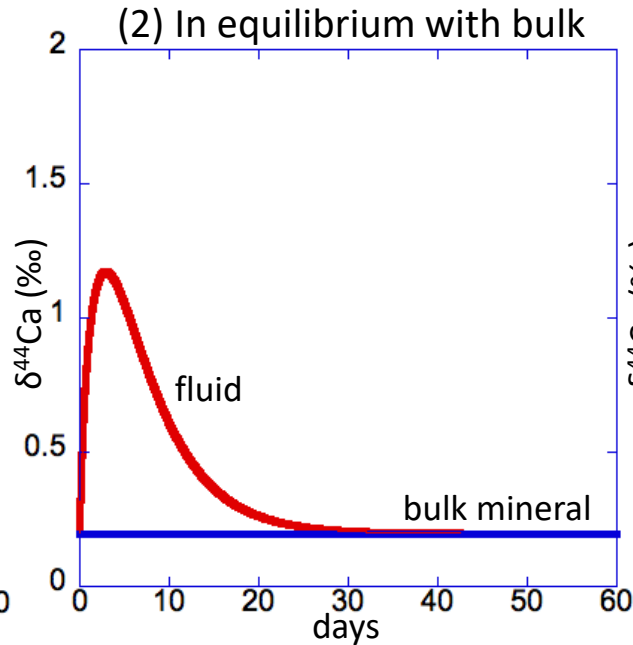
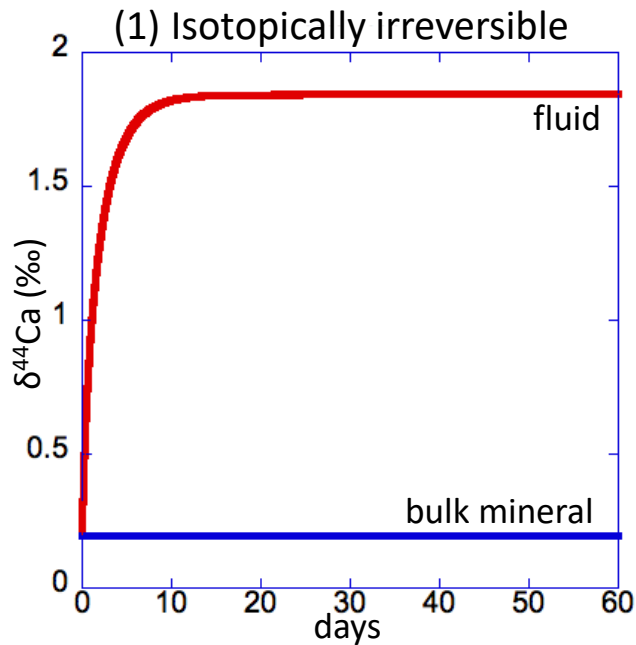


Exercise 8: Calcite precipitation with $\delta^{44}\text{Ca}$

“None”

“Bulk”

“Surface”



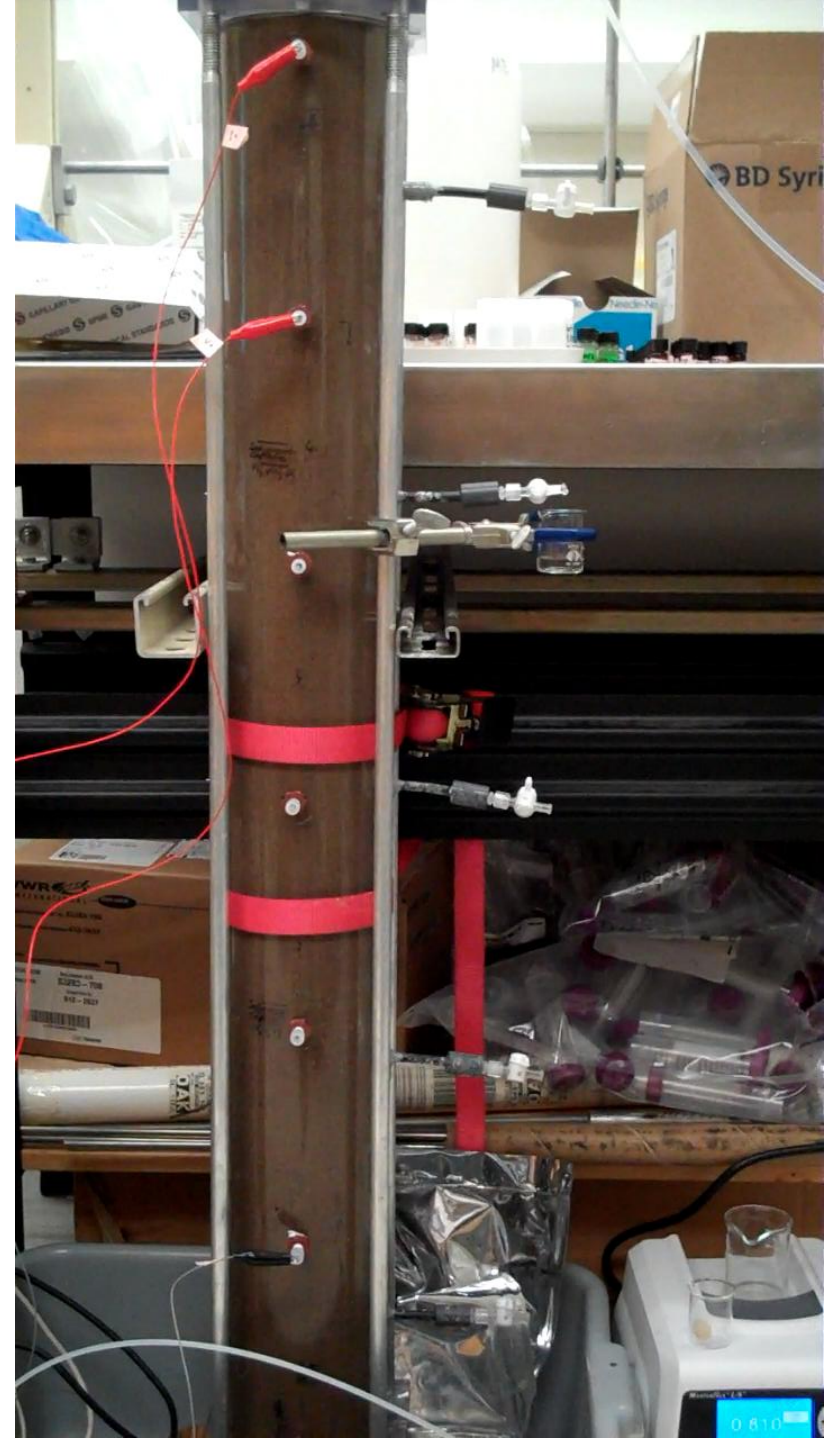
Exercise 9: Microbial Redox

Dual Monod

$$R_m = k_{\max} \left[\frac{[C_E]}{[C_E] + K_{S_E}} \frac{[C_D]}{[C_D] + K_{S_D}} \right]$$

E = electron acceptor

D = electron donor

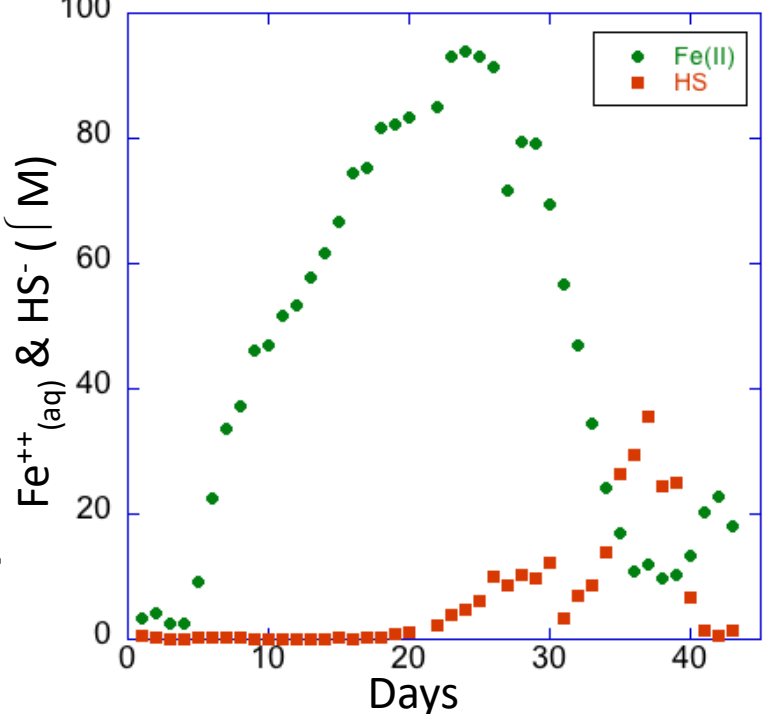
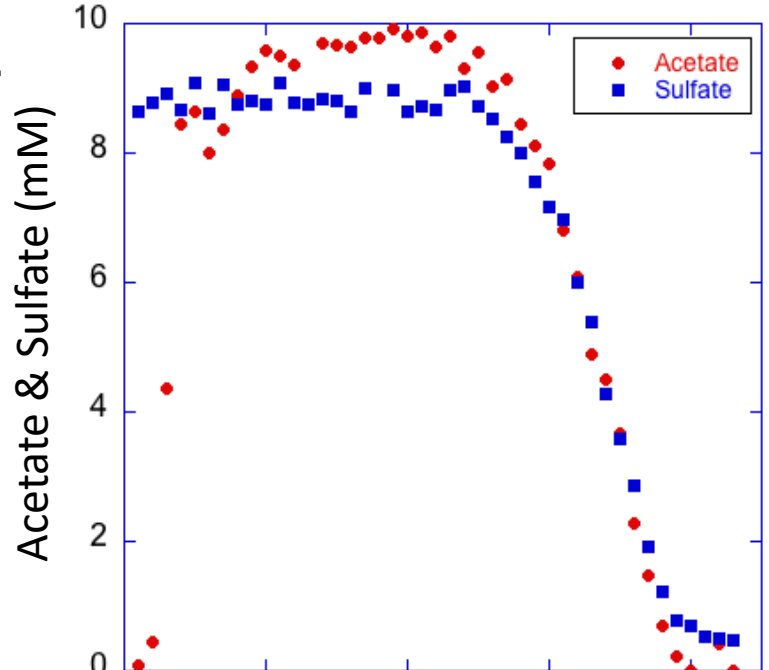


Exercise 9: Microbial Redox

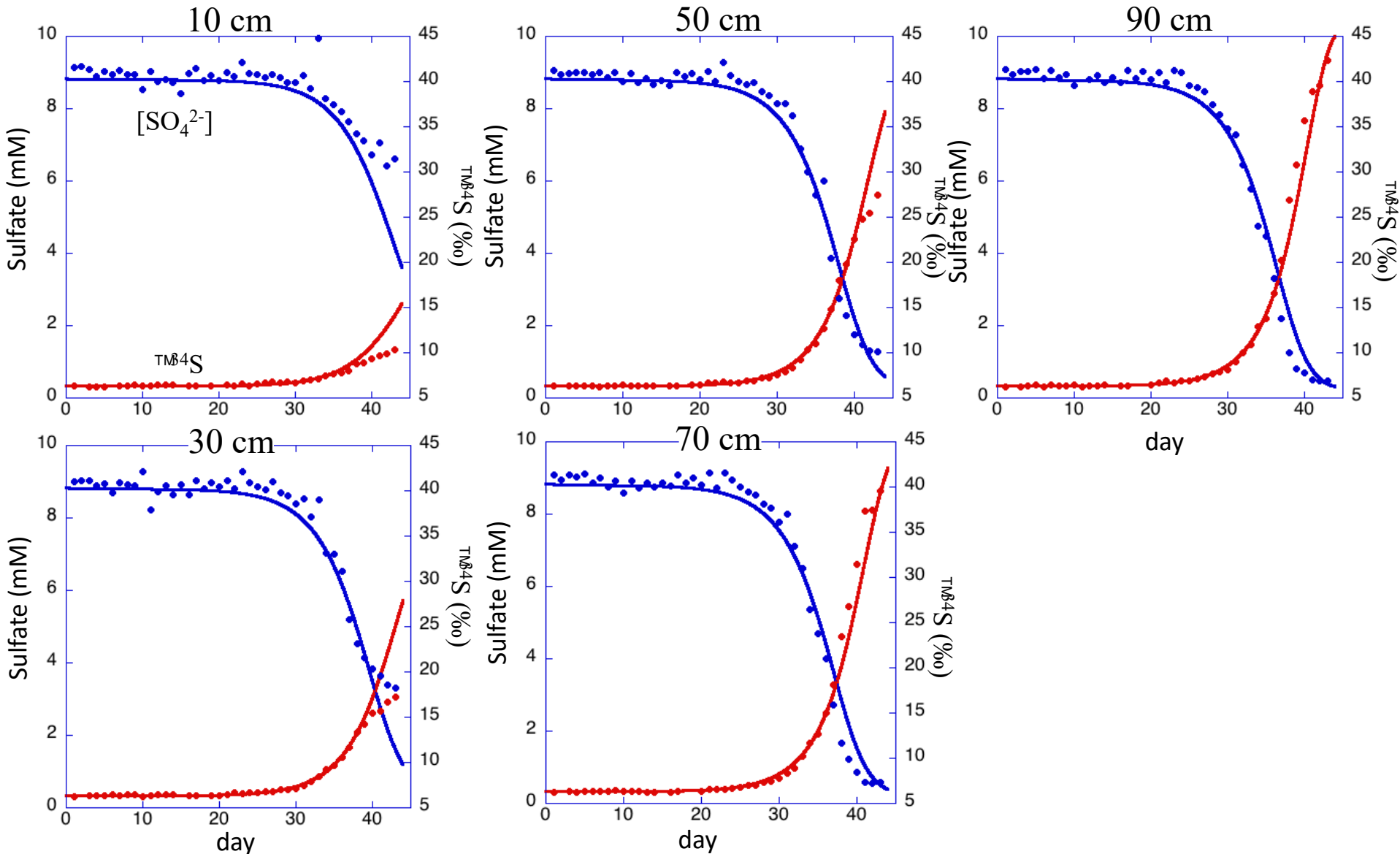


$\text{CH}_3\text{COO}^-_{(aq)}$
+ Rifle groundwater:

Uranium	0.7 – 1.5 μM
pH	7.0 – 7.2
Alkalinity	7 – 10 meq/L
Eh	-150 to 240 mV
DO	3 – 20 μM
Fe(II)	15 – 50 μM
Nitrate	2 – 3 μM
Sulfate	8 – 11 mM
Sulfide	0.03 – 0.5 μM



Exercise 9: Microbial Redox



POROSITY-PERMEABILITY CHANGE

Exercise 10: Porosity-Permeability

Mineral	Reaction	$\log K_{25}$
Calcite	$\text{Ca}^{2+} + \text{CO}_3^{2-} \leftrightarrow \text{CaCO}_3$	8.4750
Gypsum	$\text{Ca}^{2+} + \text{SO}_4^{2-} + 2\text{H}_2\text{O} \leftrightarrow \text{CaSO}_4 \cdot 2\text{H}_2\text{O}$	4.5800
Ferrihydrite	$\text{Fe}^{3+} + 3\text{H}_2\text{O} \leftrightarrow \text{Fe}(\text{OH})_3 + 3\text{H}^+$	-4.8910
Jarosite	$\text{K}^+ + 3\text{Fe}^{3+} + 2\text{SO}_4^{2-} + 6\text{H}_2\text{O} \leftrightarrow \text{KFe}_3(\text{SO}_4)_2(\text{OH})_6 + 6\text{H}^+$	9.2100
Gibbsite	$\text{Al}^{3+} + 3\text{H}_2\text{O} \leftrightarrow \text{Al}(\text{OH})_3 + 3\text{H}^+$	-8.1100
Siderite	$\text{Fe}^{2+} + \text{CO}_3^{2-} \leftrightarrow \text{FeCO}_3$	10.4500

Primary components	Unit	Initial condition	Boundary condition
pH	—	9.38	3.0
Ca^{2+}	$\text{mol l}^{-1} \text{H}_2\text{O}$	1.57×10^{-4}	1.00×10^{-4}
CO_3^{2-}	$\text{mol l}^{-1} \text{H}_2\text{O}$	2.57×10^{-4}	1.0×10^{-2}
SO_4^{2-}	$\text{mol l}^{-1} \text{H}_2\text{O}$	1.00×10^{-10}	6.46×10^{-4}

Xie, M., Mayer, K.U., Claret, F., Alt-Epping, P., Diederik, J., Steefel, C.I., Chiaberge, C., Simunek, J. (2015) Implementation and evaluation of permeability-porosity and tortuosity-porosity relationships linked to mineral dissolution-precipitation. *Computational Geosciences* **19**: 655-671. DOI 10.1007/s10596-014-9458-3

<https://wci.llnl.gov/simulation/computer-codes/visit/executables>

Exercise 10: Porosity-Permeability

```
Condition mingliang_boundary
temperature 25.0
pH 3.0
Ca++ 0.0001
CO3-- 0.01
SO4-- 0.1
Fe++ 0.000223
!!Fe++ 8.0e-3
Fe+++ 0.0143
Al+++ 0.0143
K+ 7.67e-5
O2(aq) O2(g) 0.1005
Na+ 9.092e-2
Tracer 0.01
Calcite 0.30 1.00
Gypsum 0.00 1.00
Ferrihydrite 0.00 1.00
Jarosite 0.00 1.00
Gibbsite 0.05 1.00
Siderite 0.05 1.00
TracerMineral 0.35 1.00
END
```

```
Condition initial
temperature 25.0
pH 7.0
Ca++ charge
!!Ca++ 1.69512E-04
CO3-- CO2(g) 0.01
SO4-- 1.69512E-04
Fe++ 1.0e-5
Fe+++ 1.0e-10
Al+++ 1.0e-5
K+ 1.0e-5
O2(aq) O2(g) 1.E-15
Na+ 1.0e-15
Tracer 0.00001
Calcite 0.22 1.00
Gypsum 0.00 1.00
Ferrihydrite 0.00 1.00
Jarosite 0.00 1.00
Gibbsite 0.05 1.00
Siderite 0.05 1.00
TracerMineral 0.33 1.00
END
```

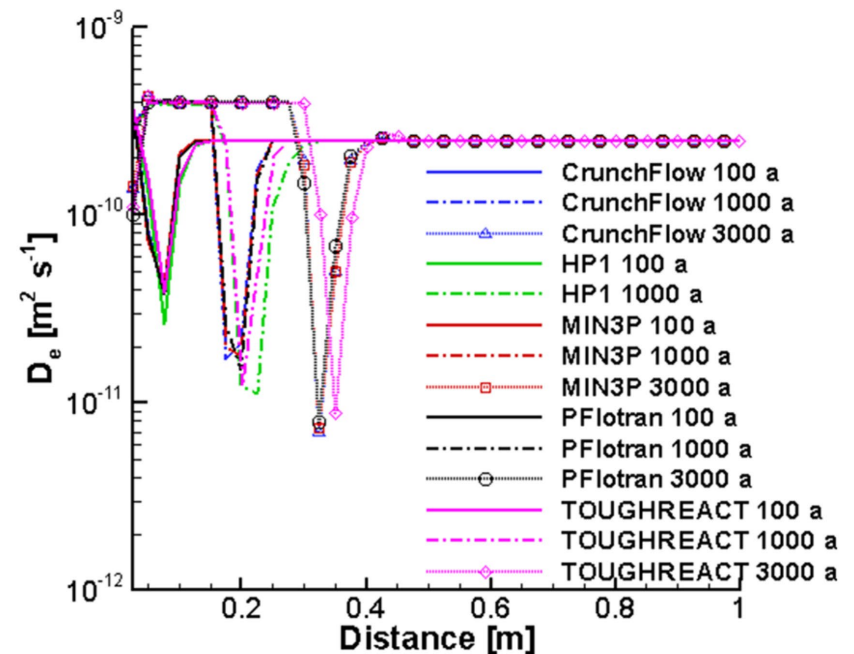
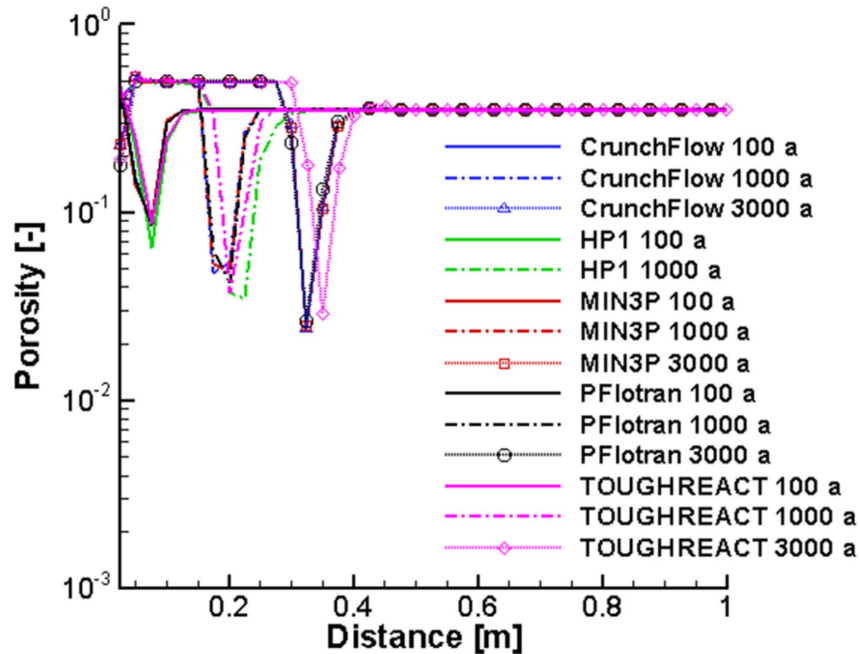
Exercise 10: 2D Porosity-Permeability

```
FLOW
distance_units  meters
time_units      second
calculate_flow   true
read_PermeabilityFile perm5_2D.hyc SingleFile3D
!!IF homogeneous flow:
!!permeability_x 1.18602E-11 default
!!permeability_x 2.61491E-10 zone 0-0 1-40 1-1
!!permeability_x 2.61491E-10 zone 31-31 1-40 1-1
permeability_y 0.00 zone 1-31 42-42 1-1
permeability_y 0.00 zone 1-31 0-0 1-1
pressure        30 default
pressure        104.4365949 zone 0-0 1-41 1-1 fix
pressure        0.0 zone 32-32 1-41 1-1 fix
gravity         90.0 90.0 90.0
END
```

```
DISCRETIZATION
distance_units meters
xzones 1 0.050 29 0.10 1 0.050
yzones 1 0.025 39 0.05 1 0.025
END
```

```
MINERALS
!! Standard linear TST calcite
Calcite      -label default -rate -4.301029996
Gypsum       -label default -rate -4.301029996
Ferrihydrite -label default -rate -5.301029996
Jarosite     -label default -rate -5.301029996
Gibbsite     -label default -rate -6.301029996
Siderite     -label default -rate -5.301029996
TracerMineral -label default -rate -35.00
END
```

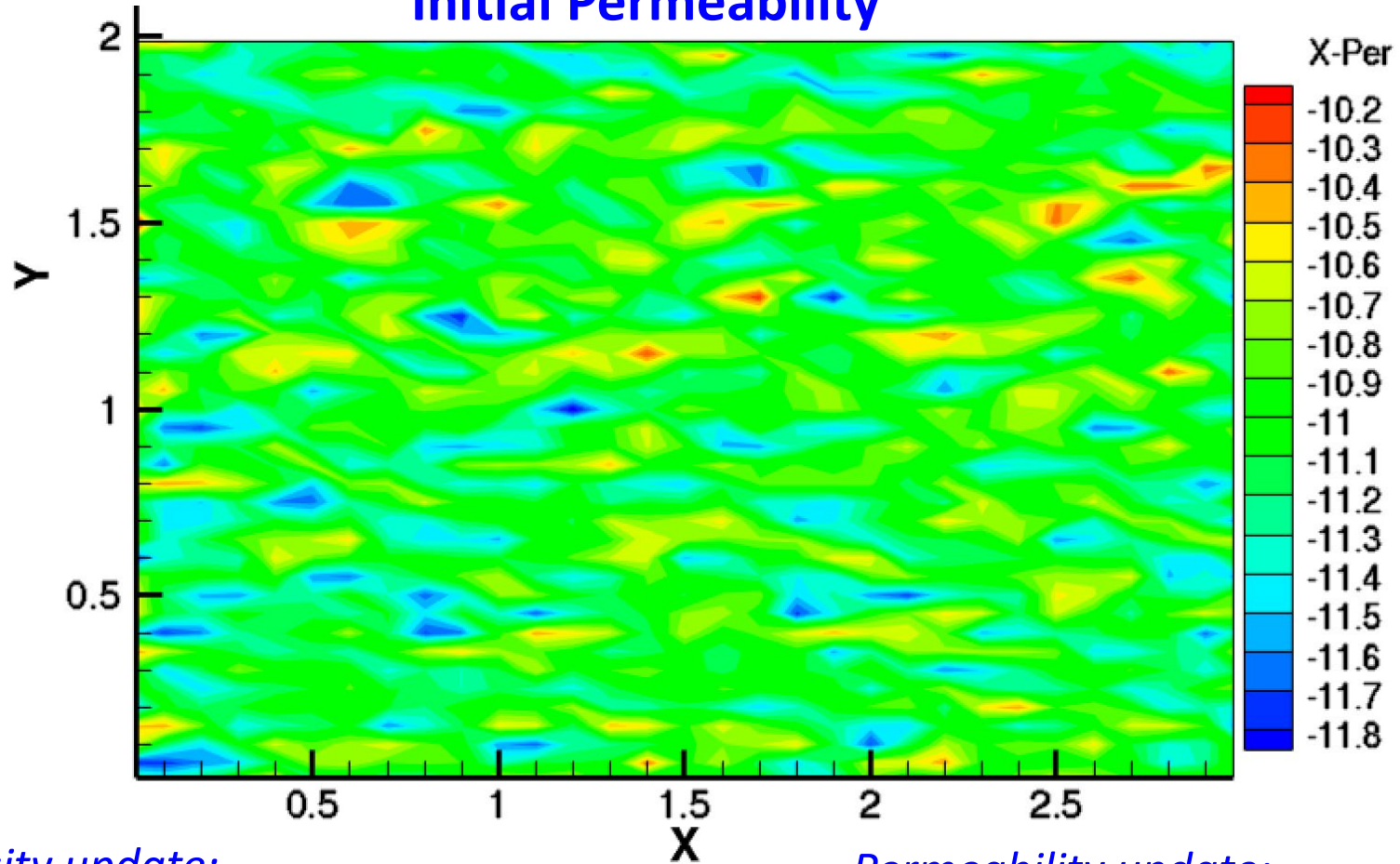
Exercise 10: 1D Porosity-Permeability



Xie et al, 2015

Exercise 10: 2D Porosity-Permeability

Initial Permeability



Porosity update:

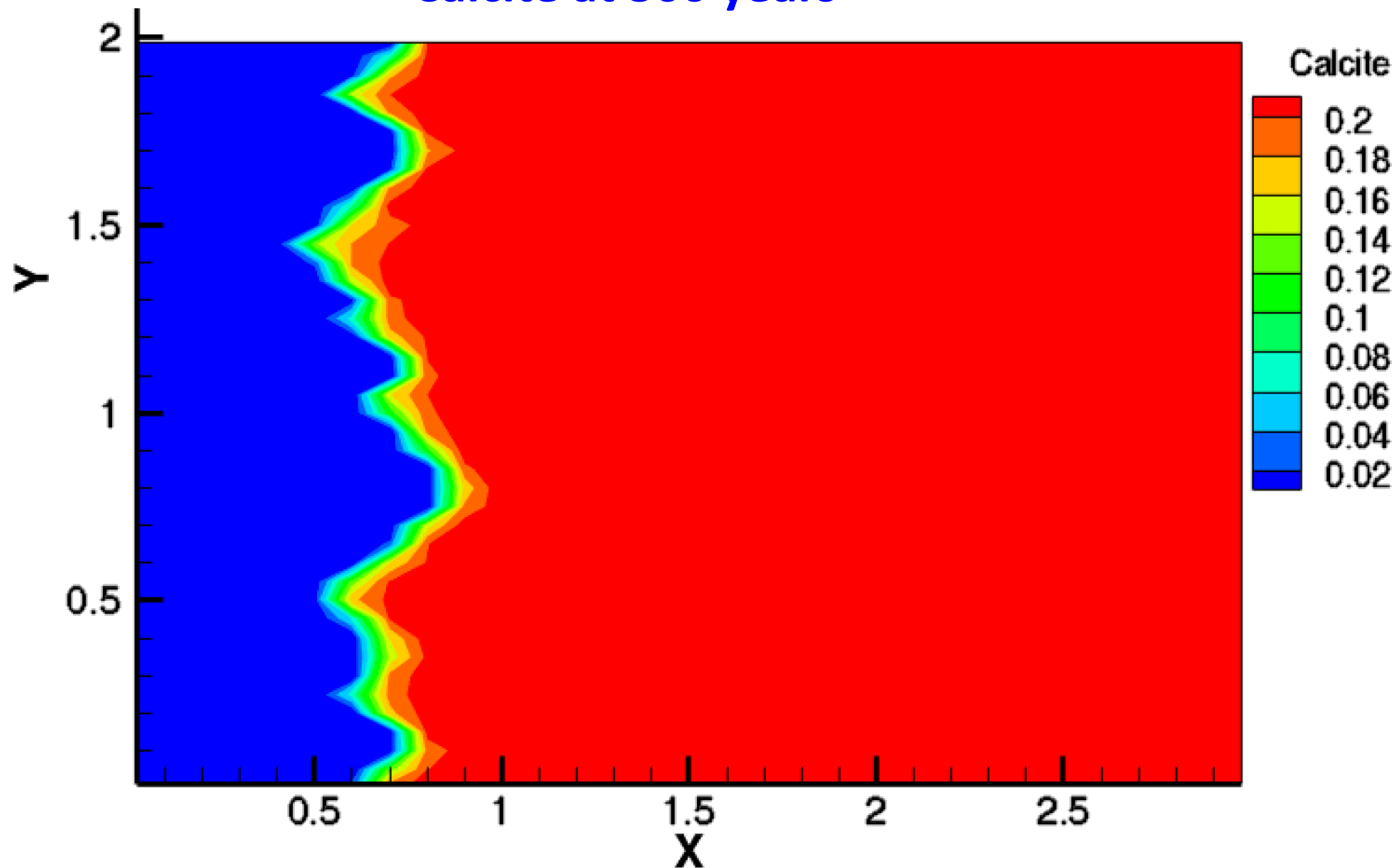
$$\phi = \sum_{m=1}^{N_m} 1 - \phi_m$$

Permeability update:

$$k_m = -k_{m,0} \left(\frac{\phi_t}{\phi_0} \right)^{2/3}$$

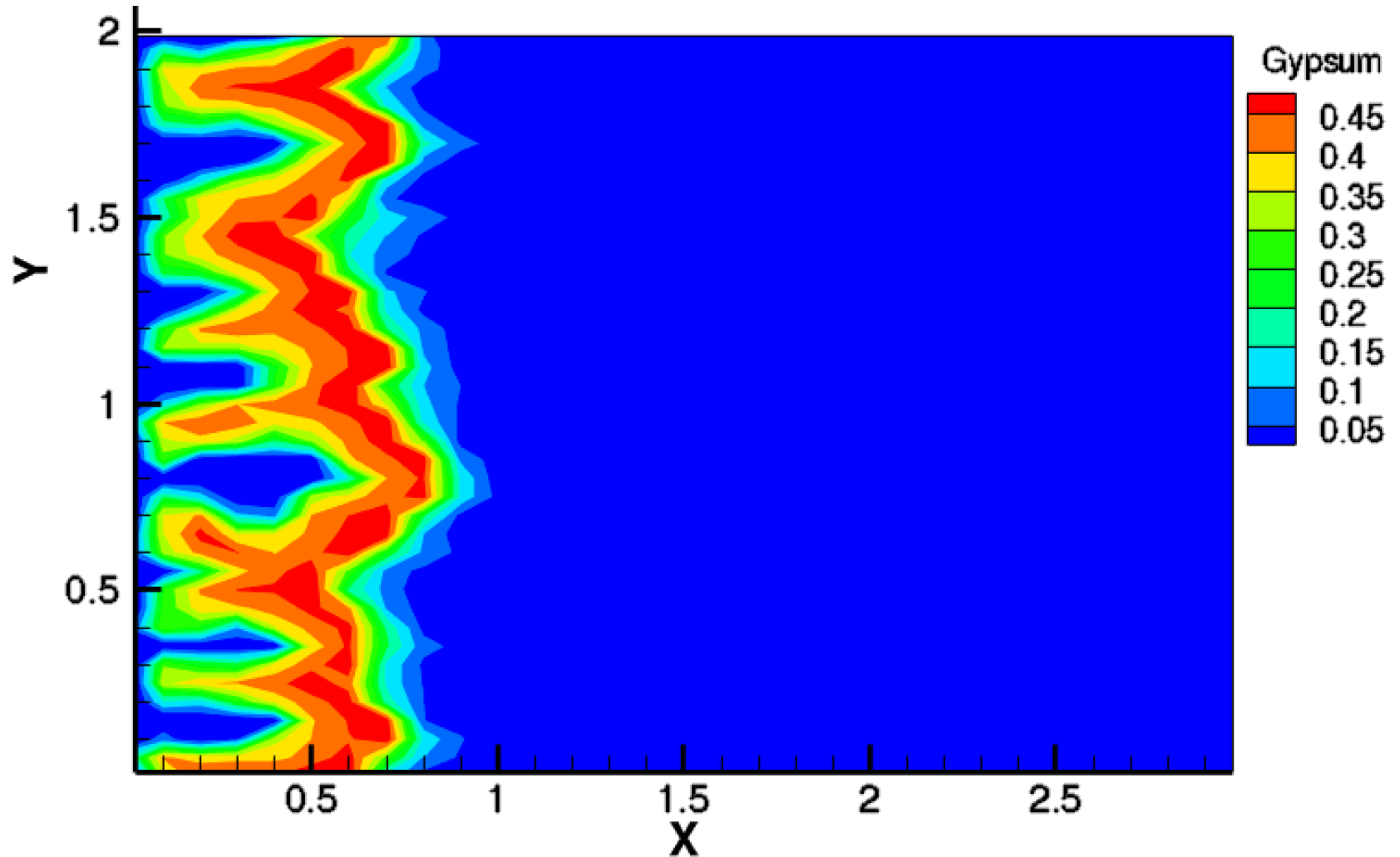
Exercise 10: 2D Porosity-Permeability

Calcite at 300 years



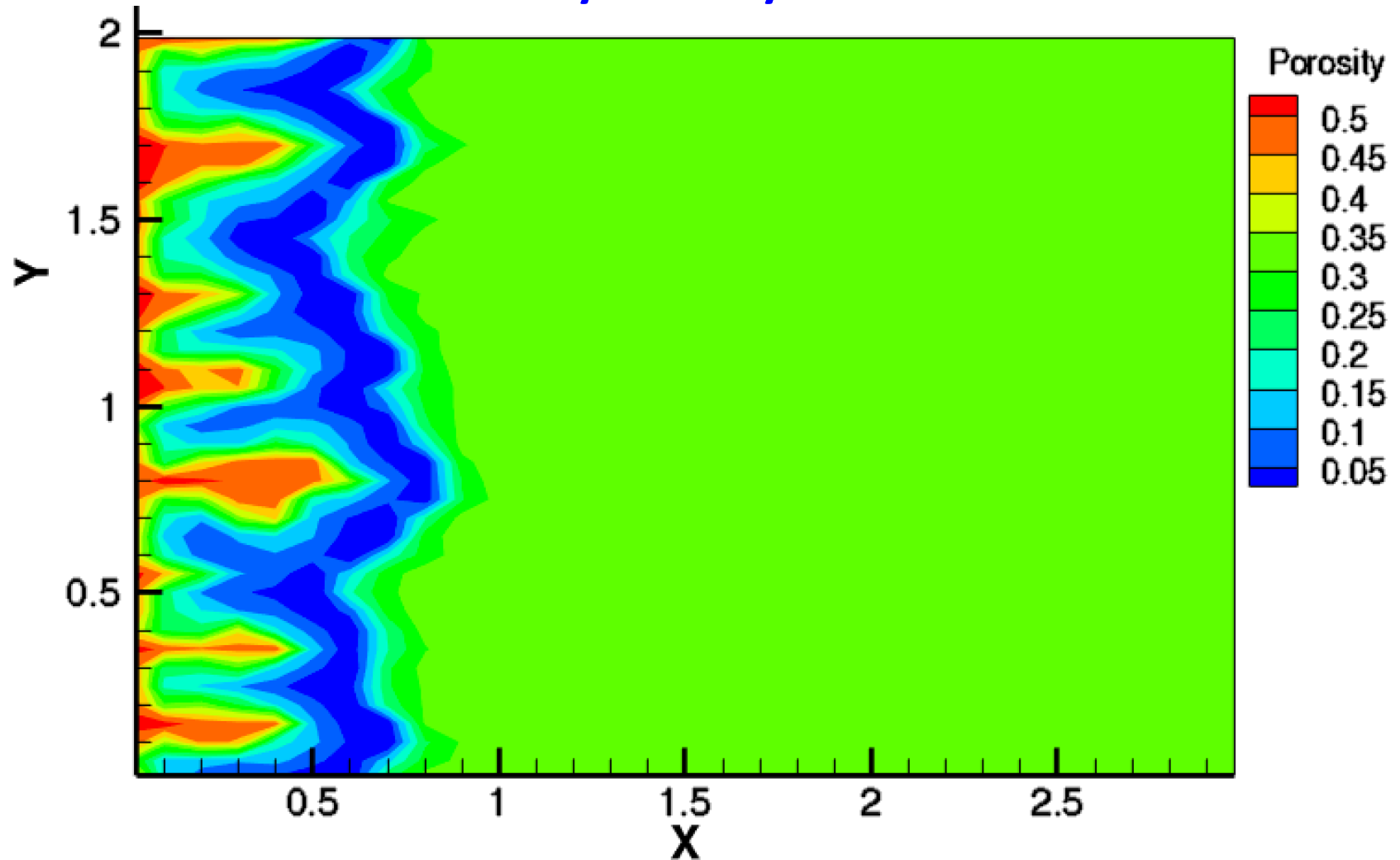
Exercise 10: 2D Porosity-Permeability

Gypsum at 300 years



Exercise 10: 2D Porosity-Permeability

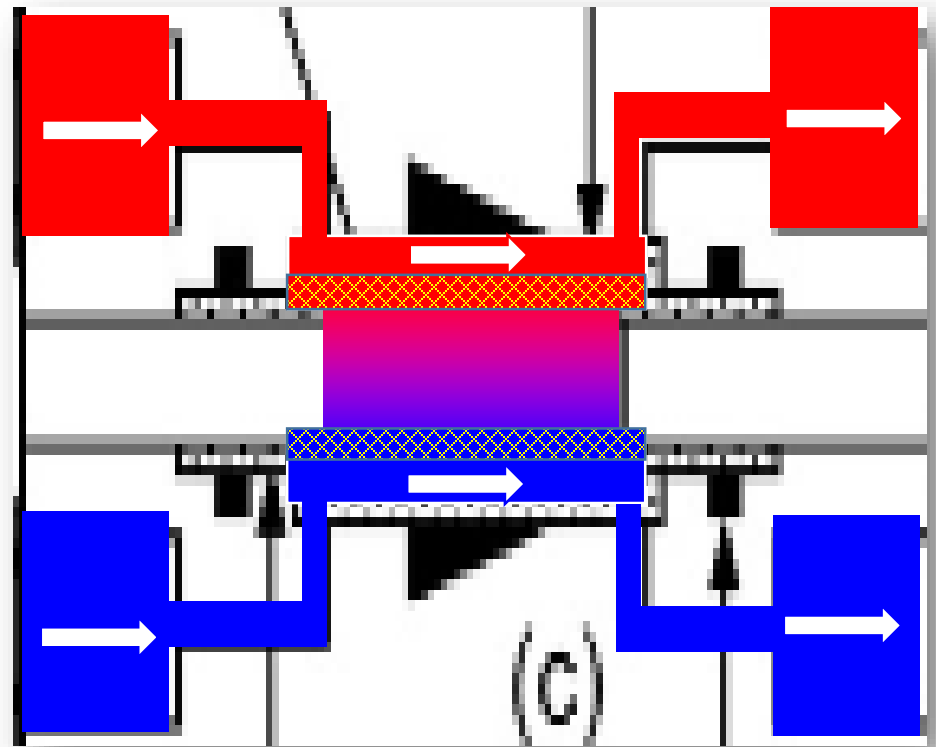
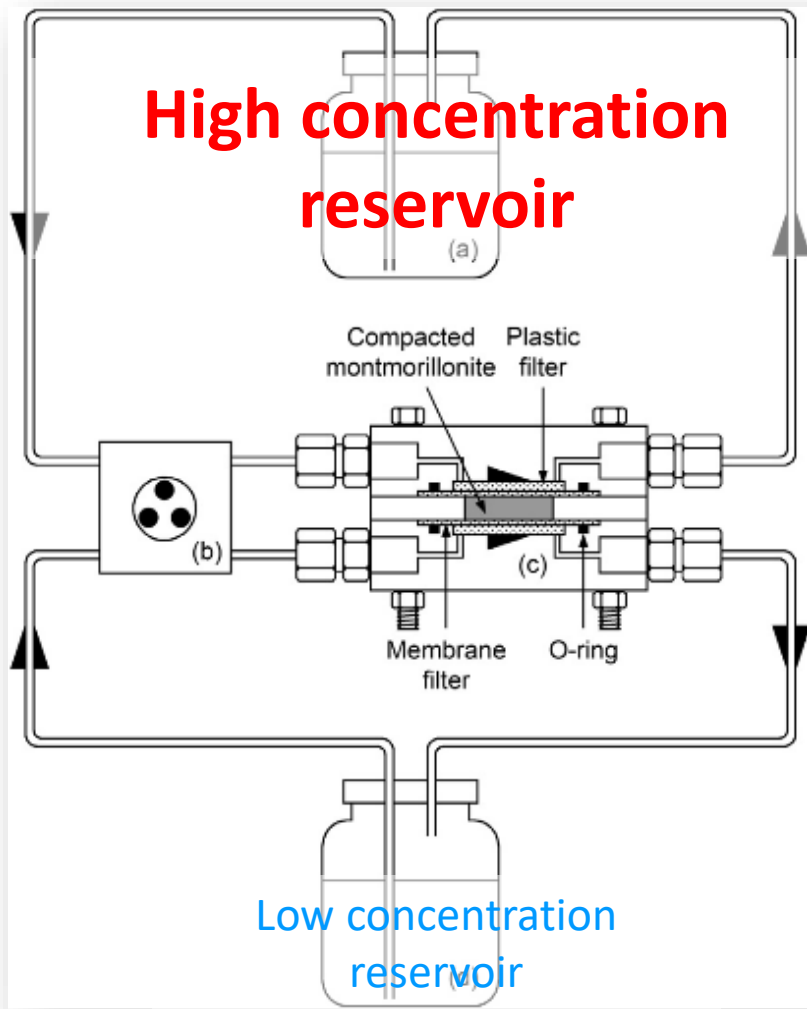
Porosity at 300 years



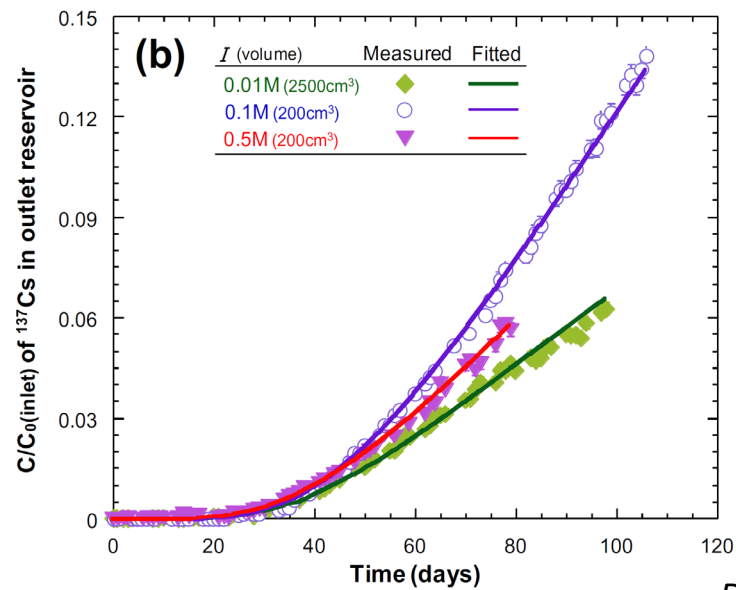
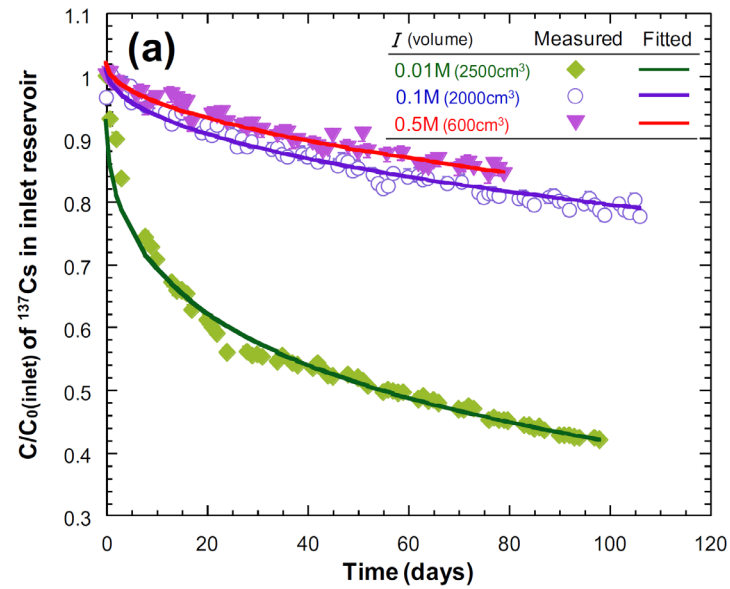
DIFFUSION IN CLAY

Exercise 11: Diffusion in Clay

Experimental setup

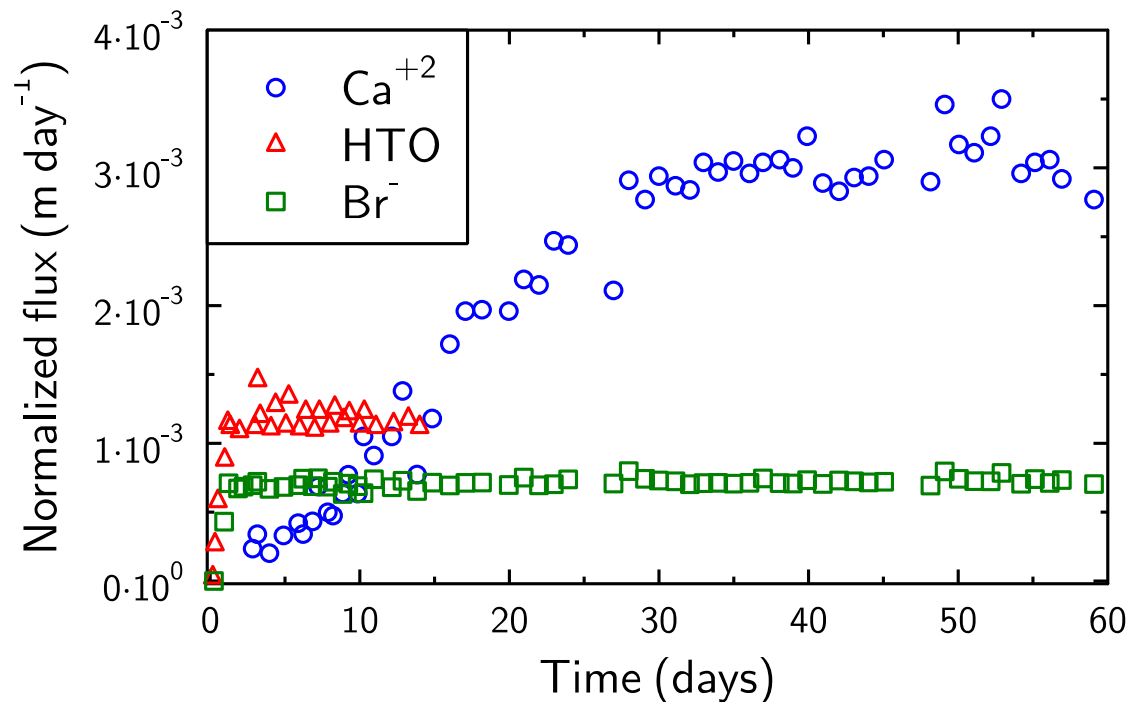


Example of results



$$Flux_{outlet} = \left. \frac{\partial C}{\partial t} \right|_{outlet} \times \frac{V_{outlet}}{S_{outlet}} \quad \text{mol m}^{-2} \text{ s}^{-1}$$

$$Flux_{norm,outlet} = \frac{Flux_{outlet}}{C_{inlet}} \quad \text{m s}^{-1}$$



Data from Tinnacher et al. GCA, 2016

Geometry of the system, general properties

DISCRETIZATION

distance_units meters

xzones 1 0.0001 50 0.0001 1 0.0001

yzones 1 100

zzones 1 1

END

Only one grid cell for the reservoir; large volume = 10 L

INITIAL_CONDITIONS

HReservoir 1-1 1-1 1-1

Clay 2-51 1-1 1-1

LReservoir 52-52 1-1 1-1

END

BOUNDARY_CONDITIONS

X_begin HReservoir Flux

X_end Lreservoir Flux

END

FLOW

space_units meters !!Default : meters ; km, cm, mm, um

time_units seconds !!Default : years ; days, hours, minutes, seconds

constant_flow 0.0 0.0 !!Default : 0.0

END

closed closed boundary conditions, only diffusion

Geometry of the system, general properties

```
POROSITY
fix_porosity      0.5
fix_microporosity 0.5
UpdateDDL        false
MultiplyPorosityTortuosity true
END
```

New keywords that are specific to CrunchClay
(ignored in CrunchTope)

```
TRANSPORT
distance_units    meters
time_units        second
fix_diffusion     1e-9

D_25 H+          9.31e-9
D_25 Bogus       1e-20
D_25 OH-         5.27e-9
D_25 Na+         1.3e-9
...

D_MP H+          9.31e-9
D_MP Bogus       1e-20
D_MP OH-         5.27e-9
D_MP Na+         1.3e-9
...
```

```
tortuosity 1 default
tortuosity 1 zone 1-1 1-1 1-1
tortuosity 0.037 zone 2-51 1-1 1-1
tortuosity 1 zone 52-52 1-1 1-1

tortuosityMP 1 default
tortuosityMP 1 zone 1-1 1-1 1-1
tortuosityMP 0.037 zone 2-51 1-1 1-1
tortuosityMP 1 zone 52-52 1-1 1-1
END
```

Chemistry, surfaces, DL properties

Condition HReservoir

```
temperature 25.0
units mmol/kg
H2O 55.5
pH 7
Na+ 100
Cl- charge
Br- 1e0
Ca++ 1e0
Hto 1e0
Bogus Bogusite
Bogusite 3.1416e-8 specific_surface_area 750
>montmor- 1e-99 !!site per m2
set_porosity 0.999999999
set_microporosity 1e-10
END
```

Background electrolyte concentration is high compared to the concentration of the tracers.

Fake mineral with very low solubility that bears the surface

The surface charge is set to zero

Redefinition of the the bulk vs DL porosity for each of the domains

The reservoirs have a porosity value of 1

Chemistry, surfaces, DL properties

Condition Clay

```
temperature 25.0
units mmol/kg
H2O 55.5
pH 7
Na+ 100
Cl- charge
Br- 1e-27
Ca++ 1e-27
Hto 1e-27
Bogus Bogusite
Bogusite 3.1416e-8 specific_surface_area 750
>montmor- 1.2e-99
set_porosity 5.655e-8
set_microporosity 5.0895e-7
END
```

Constant background electrolyte concentration

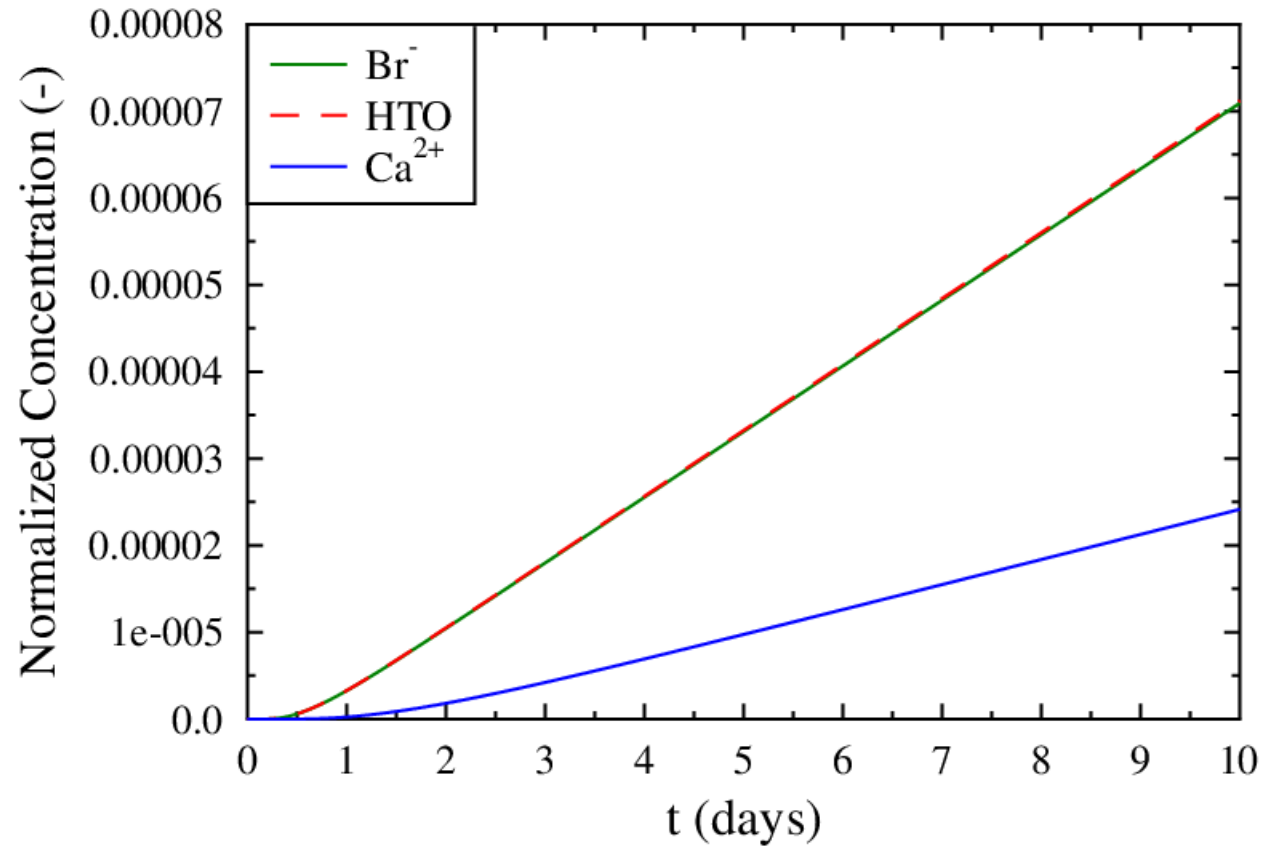
Fake mineral with very low solubility that bears the surface

The surface charge is set to zero

Redefinition of the the bulk vs DL porosity for each of the domains
See explanation in input files for calculation of these values
Here bulk porosity is 10 % of the total porosity

Results

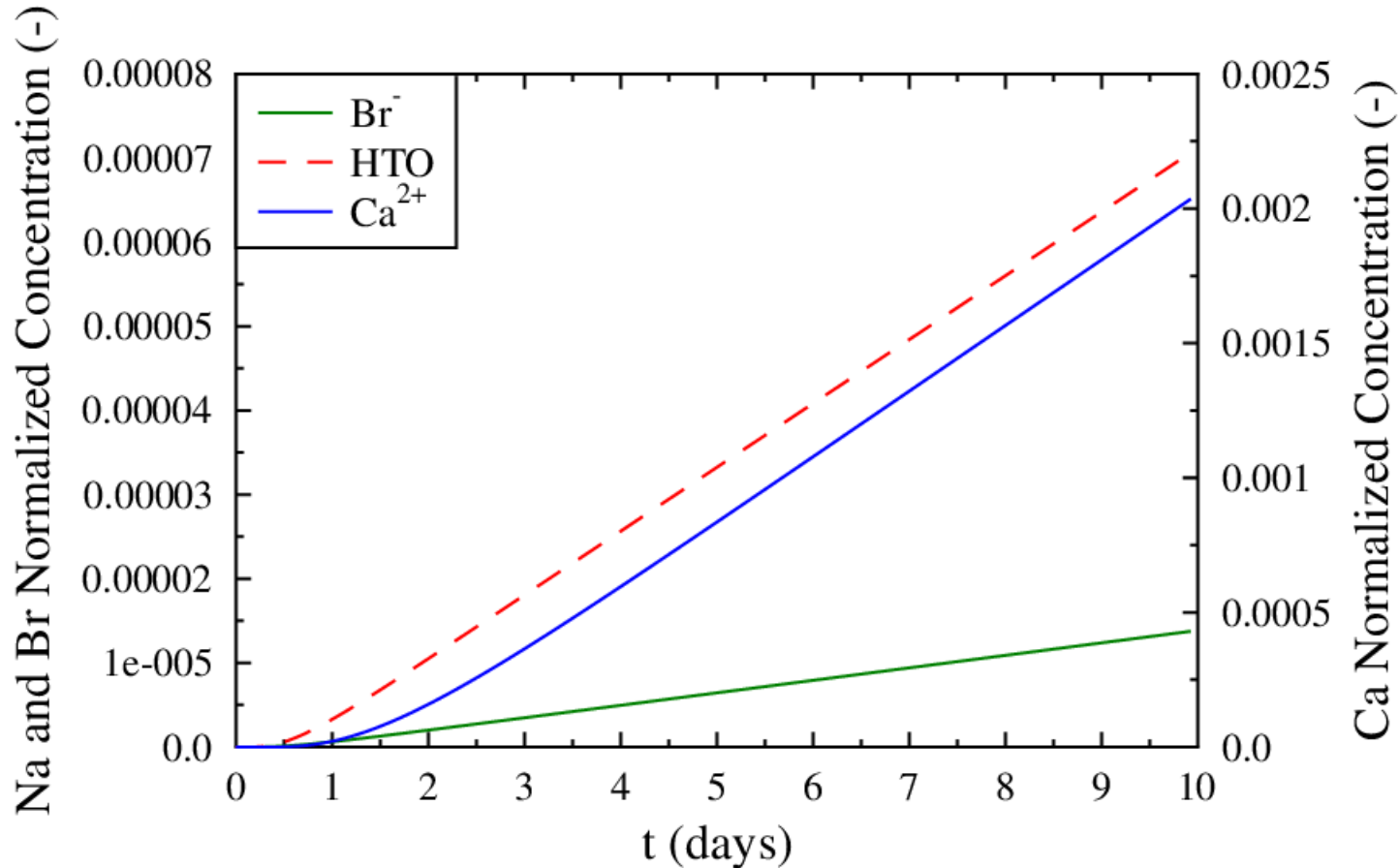
Concentration in the outlet reservoir



Why do the Br and HTO concentrations increase faster than the Ca concentration?

Results

Increase the surface charge in the clay plug to 0.9 mol charge/kg clay



What is the species that diffuse the fastest now ?

Results

Add surface complexation reactions:

```
>montmor- + Na+ = >montmorNa  
2 >montmor- + Ca+2 = > >montmor2Ca
```

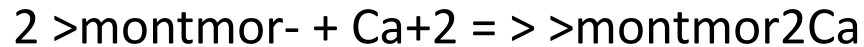
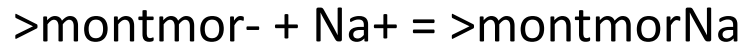
In database:

```
Begin surface complexation  
'>montmorNa' 2 1.0 'Na+' 1.0 '>montmor-' -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5  
'>montmor2Ca' 2 1.0 'Ca++' 2.0 '>montmor-' -1 -1 -1 -1 -1 -1 -1 -1  
End of surface complexation
```

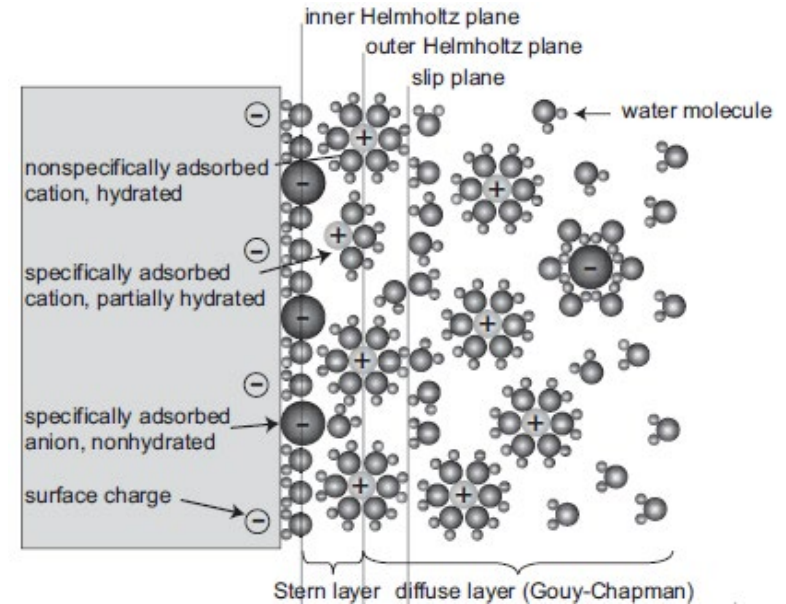
```
Begin surface complexation parameters  
>montmor- -1.0  
>montmorNa 0.0  
>montmor2Ca 0.0  
End surface complexation parameters
```

Results

Add surface complexation reactions:



The surface charge is partly compensated in the Stern layer (with no diffusion of sorbed species). The remaining charge is compensated in the diffuse layer



No surface complex

Total Charge in DDL (mol/m^3) = $5.6548800\text{E-}04$
Total Fixed Charge (mol/m^3) = $-5.6548800\text{E-}04$

Microporosity = $1.4703000000000000\text{E-}007$
DonnanPotential = $-9.386105664921650\text{E-}002$

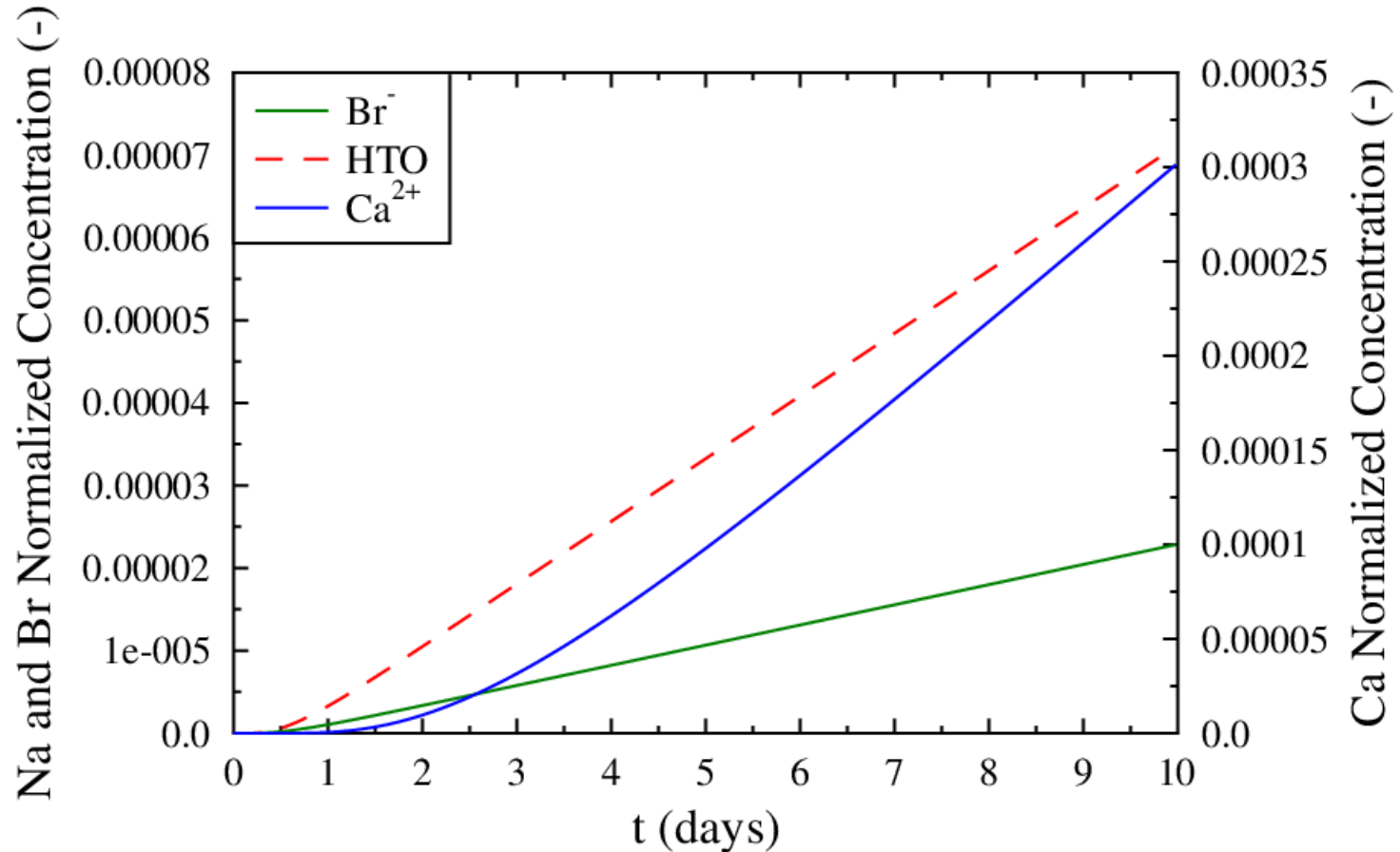
With surface complexes

Total Charge in DDL (mol/m^3) = $2.8973120\text{E-}04$
Total Fixed Charge (mol/m^3) = $-2.8973120\text{E-}04$

Microporosity = $1.4703000000000000\text{E-}007$
DonnanPotential = $-7.672779885055225\text{E-}002$

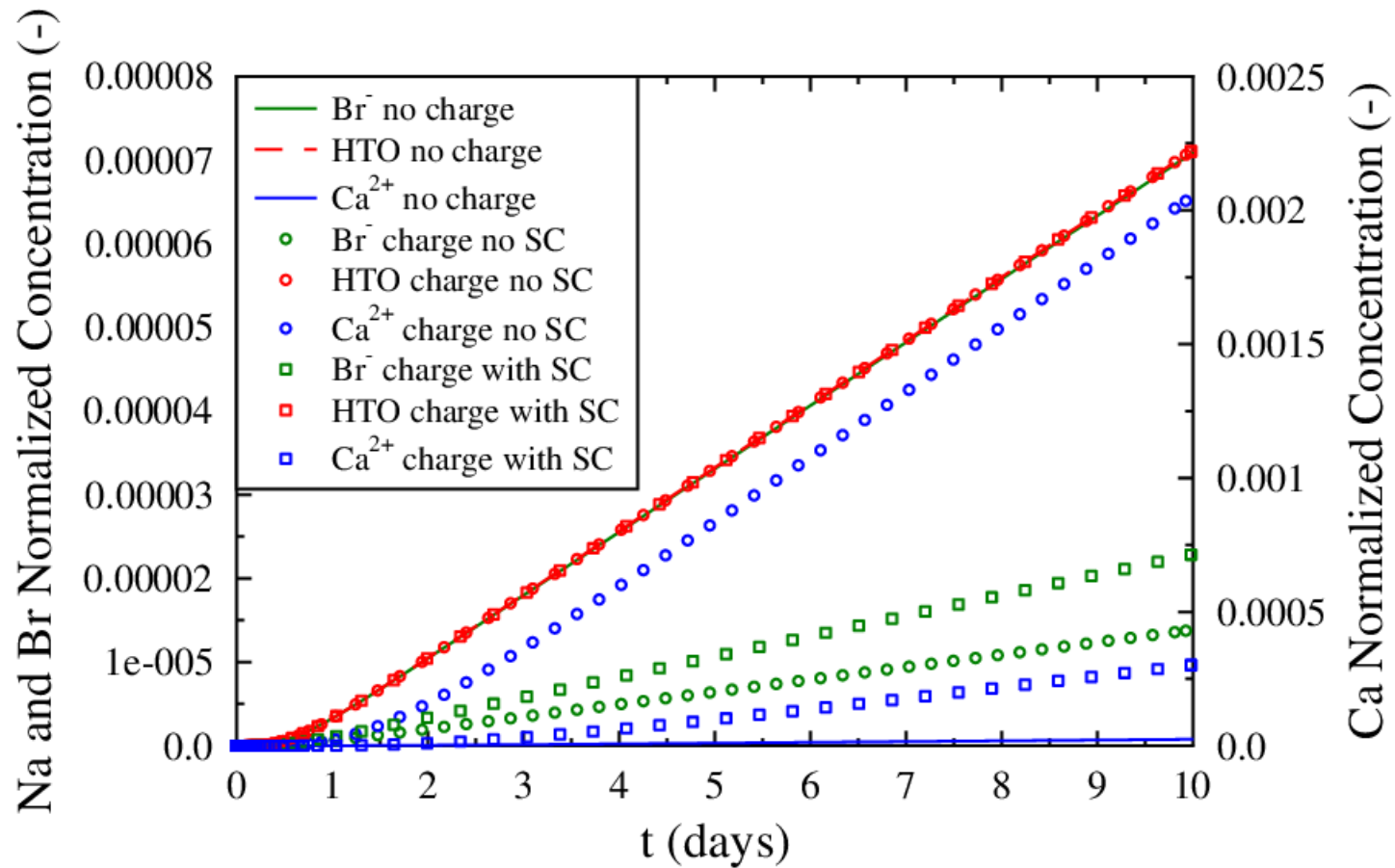
Results

Add surface complexation reactions:



What is the effect of Na and Ca surface complexation on Br and Ca diffusion?

Summary

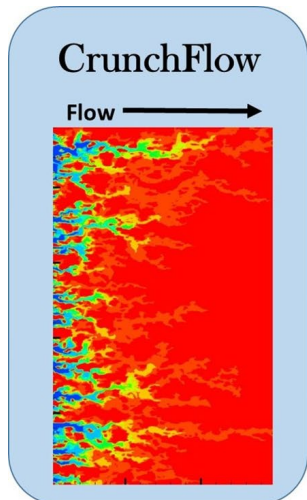


INVERSE MODELING WITH PEST-CRUNCH

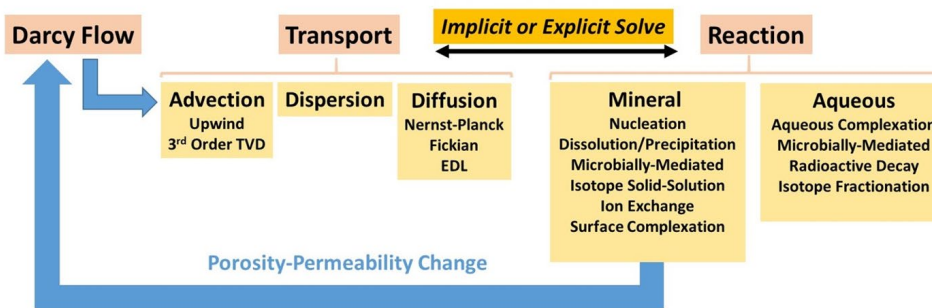
Exercise 12: Inverse Modeling with PEST-CrunchFlow

Use PEST together with CrunchFlow for inverse modeling and sensitivity analysis

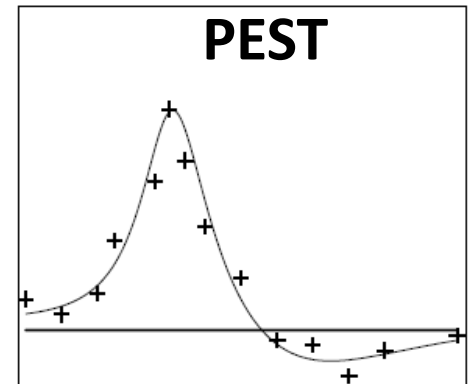
<http://www.pesthomepage.org/Home.php>



A Multicomponent Reactive Flow and Transport Simulator



<https://bitbucket.org/CrunchFlow/>



Exercise 12: Inverse Modeling with PEST-CrunchFlow

BatchNoGmin.pst File

```
pcf
* control data
restart estimation
4 165 1 0 1
1 1 double point 1 0 0
5.0 2.0 0.1 0.005 10
3.0 3.0 0.001
0.01
50 .005 4 4 .010 5
1 1 1
* group definitions and derivative data
all relative 0.01 0.0 switch 1.0 best_fit
* parameter data      Parameters
k2a none relative 0.20000 -2.0 4.0 all 1.0 0. 1
k2b none relative 0.20000 -2.0 4.0 all 1.0 0. 1
k2c none relative 0.20000 -2.0 4.0 all 1.0 0. 1
k2d none relative 0.20000 -2.0 4.0 all 1.0 0. 1
```

Number of parameters to be fitted

Number of observations

```
* observation groups
group_1
* observation data
SrCa-A11 0.00 1 group_1
SrCa-A12 0.00 1 group_1
SrCa-A13 0.00 1 group_1
SrCa-A14 42.37 1 group_1
SrCa-A15 0.05 1 group_1
SrCa-A21 1.19 1 group_1
SrCa-A22 0.56 1 group_1
SrCa-A23 0.37 1 group_1
SrCa-A24 40.50 1 group_1
SrCa-A25 0.00 1 group_1
```

```
* model command line
CrunchTopo
* model input/output
datacom-SrExchange.tpl datacom-SrExchange.dbs
PestExchange.ins PestExchange.out
```

Template file for PEST so it knows where to update parameters in CrunchTopo input file

PEST instruction file

Generated by CrunchTopo

At command line: `i64pest BatchNoGmin.pst`

Exercise 12: Inverse Modeling with PEST-CrunchFlow

PestExchange.out File

Primary Species	uEquiv/kgw	uEquiv/g solid
Ca++	3.6555E+01	1.8278E-01
K+	1.2860E+02	6.4298E-01
Mg++	9.7581E+00	4.8791E-02
Sr++	8.2991E+03	4.1495E+01
Na+	6.0143E+00	3.0071E-02
Primary Species	uEquiv/kgw	uEquiv/g solid
Ca++	2.2798E+02	1.1399E+00
K+	2.0261E+02	1.0131E+00
Mg++	9.6190E+00	4.8095E-02
Sr++	8.0784E+03	4.0392E+01
Na+	1.3673E+00	6.8364E-03

Generated by CrunchTape per instructions in
BatchNoGmin.in file

PestExchange.ins File

```
pif @  
l2 [srca-a11]34:44  
l1 [srca-a12]34:44  
l1 [srca-a13]34:44  
l1 [srca-a14]34:44  
l1 [srca-a15]34:44  
l2 [srca-a21]34:44  
l1 [srca-a22]34:44  
l1 [srca-a23]34:44  
l1 [srca-a24]34:44  
l1 [srca-a25]34:44
```

Tells PEST where to find
the simulation data in
PestExchange.out
file to compare to
observations

Datacom-SrExchange.tpl File

'Sr-XB8814-2'	2	1.0	'Sr++'	2.0	'XB8814-2'	0.00	0.000
'Ca-XB8814-2'	2	1.0	'Ca++'	2.0	'XB8814-2'	#k2a	# 0.000
'Na-XB8814-2'	2	1.0	'Na+'	1.0	'XB8814-2'	#k2b	# 0.000
'Mg-XB8814-2'	2	1.0	'Mg++'	2.0	'XB8814-2'	#k2c	# 0.000
'K-XB8814-2'	2	1.0	'K+'	1.0	'XB8814-2'	#k2d	# 0.000
End of exchange							

Datacom-SrExchange.dbs File

'Sr-XB8814-2'	2	1.0	'Sr++'	2.0	'XB8814-2'	0.00	0.000
'Ca-XB8814-2'	2	1.0	'Ca++'	2.0	'XB8814-2'	.0918334263	0.000
'Na-XB8814-2'	2	1.0	'Na+'	1.0	'XB8814-2'	-.909927443	0.000
'Mg-XB8814-2'	2	1.0	'Mg++'	2.0	'XB8814-2'	.1465642933	0.000
'K-XB8814-2'	2	1.0	'K+'	1.0	'XB8814-2'	-1.88939379	0.000
End of exchange							

Exercise 12: Inverse Modeling with PEST-CrunchFlow

BatchNoGmin.rec File

OPTIMISATION RESULTS

Parameters ----->

Parameter	Estimated	95% percent confidence limits	
	value	lower limit	upper limit
k2a	9.183343E-02	8.310404E-02	0.100563
k2b	-0.909927	-1.47566	-0.344194
k2c	0.146564	0.127452	0.165677
k2d	-1.88939	-1.96078	-1.81801

Note: confidence limits provide only an indication of parameter uncertainty.

They rely on a linearity assumption which may not extend as far in

parameter space as the confidence limits themselves - see PEST manual.

See file batchnogmin.sen for parameter sensitivities.

Observation	Measured	Calculated	Residual	Weight
	value			
srca-a11	0.00000	0.182780	-0.182780	1.000
srca-a12	0.00000	0.642980	-0.642980	1.000
srca-a13	0.00000	4.879100E-02	-4.879100E-02	1.000
srca-a14	42.3700	41.4950	0.875000	1.000
srca-a15	5.000000E-02	3.007100E-02	1.992900E-02	1.000
srca-a21	1.19000	1.13990	5.010000E-02	1.000
srca-a22	0.560000	1.01310	-0.453100	1.000
srca-a23	0.370000	4.809500E-02	0.321905	1.000
srca-a24	40.5000	40.3920	0.108000	1.000
srca-a25	0.00000	6.836400E-03	-6.836400E-03	1.000

Find summary of optimization results in *.rec file generated by PEST

Numerical Approach

Derivative of Total Concentration

$$\psi_i = C_i + \sum_{l=1}^{N_s} \nu_{i,l} C_l = C_i + \sum_{l=1}^{N_s} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right]$$

The derivative of the total concentration with respect to the primary species concentrations

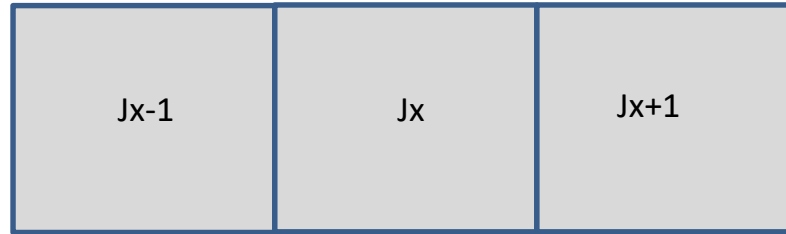
$$\frac{\partial}{\partial C_k} \left\{ \left[\psi_{i,jx}^{n+1} \right] \right\} = \frac{\partial}{\partial C_k} \left\{ C_i + \sum_{l=1}^{N_s} \nu_{i,l} C_l \right\} = \delta_{i,k} + \sum_{l=1}^{N_s} \left(\frac{\nu_{k,l}}{C_k} \right) \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right]$$

Or using the logarithms of the concentrations as the primary unknowns (which scales the Jacobian matrix, making it numerically more tractable)

$$d \ln X = \frac{dX}{X}$$

$$\frac{\partial}{\partial \ln C_k} \left\{ \left[\psi_{i,jx}^{n+1} \right] \right\} = \delta_{i,k} C_i + \sum_{l=1}^{N_s} \nu_{k,l} \nu_{i,l} \left[\prod C_p^{\nu_{p,l}} K_{eq}^{-1} \right] = \delta_{i,k} C_i + \sum_{l=1}^{N_s} \nu_{k,l} \nu_{i,l} C_l$$

Jacobian Matrix for Global Implicit Method



Jx

$$\frac{\phi}{\Delta t} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx}^{n+1} + \frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx}^{n+1} +$$

$$2 \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx}^{n+1}$$

Jx-1

$$- \frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx-1}^{n+1} - \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx-1}^{n+1}$$

Jx+1

$$- \frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx+1}^{n+1} - \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx+1}^{n+1}$$

Newton's Method for Global Implicit Method

$$\begin{aligned}
 & \frac{\phi}{\Delta t} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx}^{n+1} \\
 & + \frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx}^{n+1} + 2 \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx}^{n+1} \\
 & - \frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx-1}^{n+1} - \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx-1}^{n+1} \\
 & - \frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx+1}^{n+1} - \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,jx+1}^{n+1} =
 \end{aligned}$$

Nc x Nc Jacobian Submatrix

$$\left\{ \begin{aligned}
 & \phi \frac{\left[C_i + \sum_{l=1}^{N_s} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right]_{i,jx}^{n+1} - \psi_{i,jx}^n \right]}{\Delta t} \\
 & - \phi D \frac{\left[\left(C_i + \sum_{l=1}^{N_s} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right]_{i,jx-1}^{n+1} \right) - 2 \left(C_i + \sum_{l=1}^{N_s} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right]_{i,jx}^{n+1} \right) + \left(C_i + \sum_{l=1}^{N_s} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right]_{i,jx+1}^{n+1} \right) \right]}{\Delta x^2} \\
 & + \phi v \frac{\left[\left(C_i + \sum_{l=1}^{N_s} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right]_{i,jx}^{n+1} \right) - \left(C_i + \sum_{l=1}^{N_s} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right]_{i,jx-1}^{n+1} \right) \right]}{\Delta x}
 \end{aligned} \right.$$

Nc Residual Vectors

Newton's Method for Global Implicit

For $JX = 2$

$$\begin{aligned} \mathbf{Nc} \times \mathbf{Nc} \quad \mathbf{A}_{22} &= \frac{\phi}{\Delta t} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,2}^{n+1} + \frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,2}^{n+1} \\ &+ 2 \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,2}^{n+1} \end{aligned}$$

$$\mathbf{Nc} \times \mathbf{Nc} \quad \mathbf{A}_{21} = -\frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,1}^{n+1} - \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,1}^{n+1}$$

$$\mathbf{Nc} \times \mathbf{Nc} \quad \mathbf{A}_{21} = -\frac{\phi v}{\Delta x} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,3}^{n+1} - \frac{\phi D}{\Delta x^2} \left[\delta_{i,k} C_i + \sum_{l=1}^{N_s} v_{k,l} v_{i,l} \left[\Pi C_p^{v_{p,l}} K_{eq}^{-1} \right] \right]_{i,3}^{n+1}$$

$$\begin{bmatrix} A_{1,1} & A_{1,2} & 0 & \cdots \\ A_{2,1} & A_{2,2} & A_{2,3} & \cdots \\ & & & \cdots \\ & & & \cdots & A_{N-1,N-2} & A_{N-1,N-1} & A_{N-1,N} \\ & & & \cdots & 0 & A_{N,N-1} & A_{N,N} \end{bmatrix} \begin{bmatrix} \delta C_1 \\ \delta C_2 \\ \cdots \\ \delta C_{N-1} \\ \delta C_N \end{bmatrix} = - \begin{bmatrix} f_1 \\ f_2 \\ \cdots \\ f_{N-1} \\ f_N \end{bmatrix}$$